



# **Thermoelectrics in Space: A Success Story, What's Next and What Might Be Possible**

***KISS Adaptive Multi-Functional Systems - Part II  
California Institute of Technology***

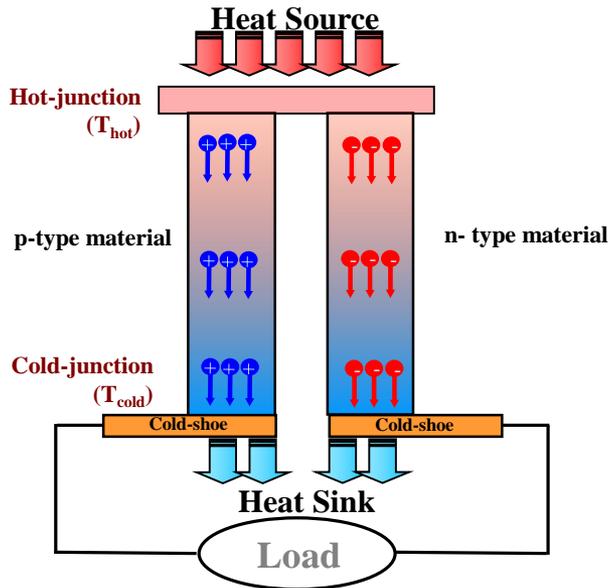
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Pasadena, California, USA**

**February 17, 2015**

# Thermoelectric Power Generation

## Thermoelectric Couple



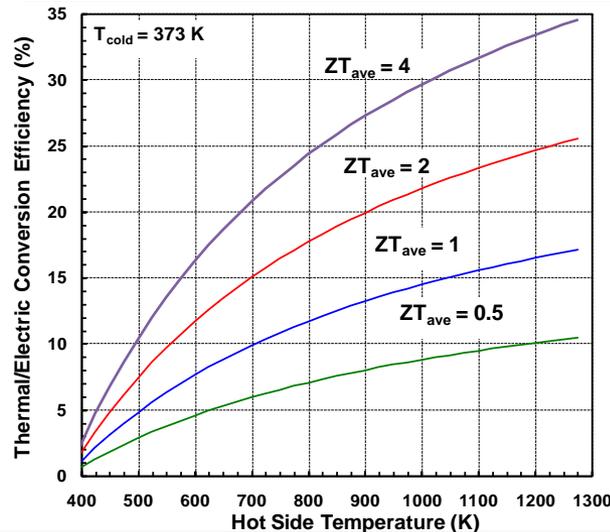
## Dimensionless Thermoelectric Figure of Merit, ZT

$$ZT = \frac{\sigma S^2 T}{\lambda} = \frac{S^2 T}{\rho \lambda}$$

Seebeck coefficient  $S$   
 Electrical conductivity  $\sigma$   
 Electrical resistivity  $\rho$   
 Thermal conductivity  $\lambda$   
 Absolute temperature  $T$

$$\eta_{\text{max}} = \frac{\text{Carnot}}{\text{TE Materials}} = \frac{T_{\text{ht}} - T_{\text{cld}}}{T_{\text{ht}}} \frac{\sqrt{1+ZT} - 1}{\sqrt{1+ZT} + \frac{T_{\text{cld}}}{T_{\text{ht}}}}$$

## Conversion Efficiency



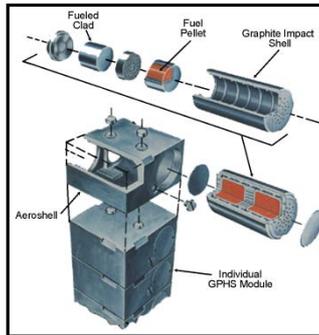
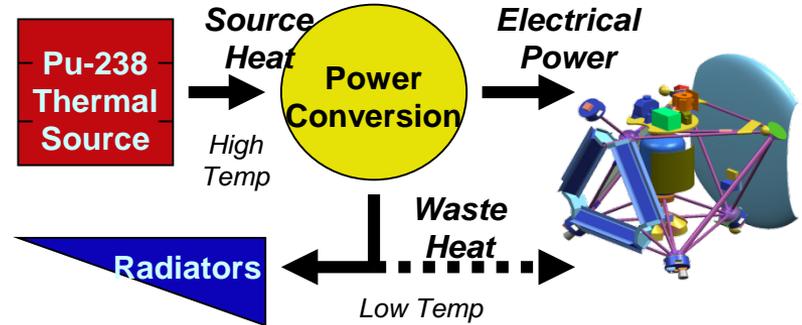
*Power generation*  
 (across 1275 to 300 K)  
 State-Of-Practice materials:  
 $ZT_{\text{average}} \sim 0.5$   
 State-Of-the-Art materials:  
 $ZT_{\text{average}} \sim 1.2$   
 Best SOA materials:  
 $ZT_{\text{peak}} \sim 2.6$

Thermoelectric effects are defined by a coupling between the electrical and thermal currents induced by an electric field and a temperature gradient

Conversion efficiency is a direct function of  $ZT_{\text{ave}}$  and  $\Delta T$

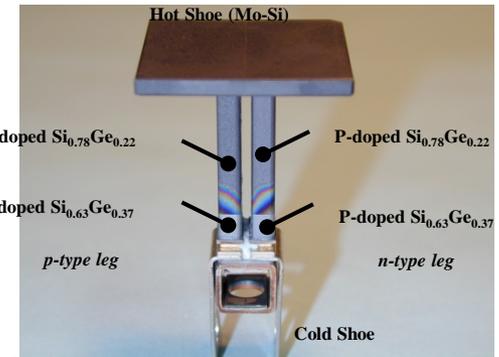
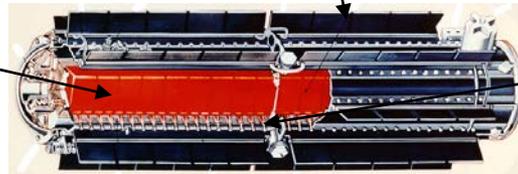
# RTG Technology - What is a RTG?

**RTG is a thermoelectric conversion system that converts heat produced from natural alpha ( $\alpha$ ) particle decay of plutonium into electrical energy (DC)**



*Heat Source Assembly (GPHS Modules)*

*Housing & Radiator Assembly*



*Thermoelectric couple (572 couples used in the GPHS-RTG)*

**GPHS-Radioisotope Thermoelectric Generator (RTG)**

# Historical RTG-Powered U.S. Missions



Mission	RTG type (number)	TE	Destination	Launch Year	Mission Length	Power Level*
Transit 4A	SNAP-3B7(1)	PbTe	Earth Orbit	1961	15	2.7
Transit 4B	SNAP-3B8 (1)	PbTe	Earth Orbit	1962	9	2.7
Nimbus 3	SNAP-19 RTG (2)	PbTe	Earth Orbit	1969	> 2.5	~ 56
Apollo 12 <sup>#</sup>	SNAP-27 RTG (1)	PbTe	Lunar Surface	1969	8	~ 70
Pioneer 10	SNAP-19 RTG (4)	PbTe	Outer Planets	1972	34	~ 160
Triad-01-1X	SNAP-9A (1)	PbTe	Earth Orbit	1972	15	~ 35
Pioneer 11	SNAP-19 RTG (4)	PbTe	Outer Planets	1973	35	~ 160
Viking 1	SNAP-19 RTG (2)	PbTe	Mars Surface	1975	> 6	~ 84
Viking 2	SNAP-19 RTG (2)	PbTe	Mars Surface	1975	> 4	~ 84
LES 8	MHW-RTG (2)	Si-Ge	Earth Orbit	1976	15	~ 308
LES 9	MHW-RTG (2)	Si-Ge	Earth Orbit	1976	15	~ 308
Voyager 1	MHW-RTG (3)	Si-Ge	Outer Planets	1977	37	~475
Voyager 2	MHW-RTG (3)	Si-Ge	Outer Planets	1977	37	~475
Galileo	GPHS-RTG (2)	Si-Ge	Outer Planets	1989	14	~ 574
Ulysses	GPHS-RTG (1)	Si-Ge	Outer Planets/Sun	1990	18	~ 283
Cassini	GPHS-RTG (3)	Si-Ge	Outer Planets	1997	11	~ 885
New Horizons	GPHS-RTG (1)	Si-Ge	Outer Planets	2005	9 (17)	~ 246
MSL	MMRTG (1)	PbTe	Mars Surface	2011	3 (to date)	~ 115
<i>Mars 2020**</i> <small>Apollo 12, 14, 15, 16 and 17</small>	<i>MMRTG (1 baselined)</i>	<i>PbTe</i>	<i>Mars Surface</i>	<i>2020</i>	<i>(5)</i>	<i>&gt; 110</i>

\*Total power at Beginning of Mission (W)

\*\*Planned

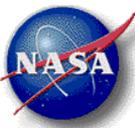
RTGs have been successfully used on a number of long-life missions



# The Success Story to Date

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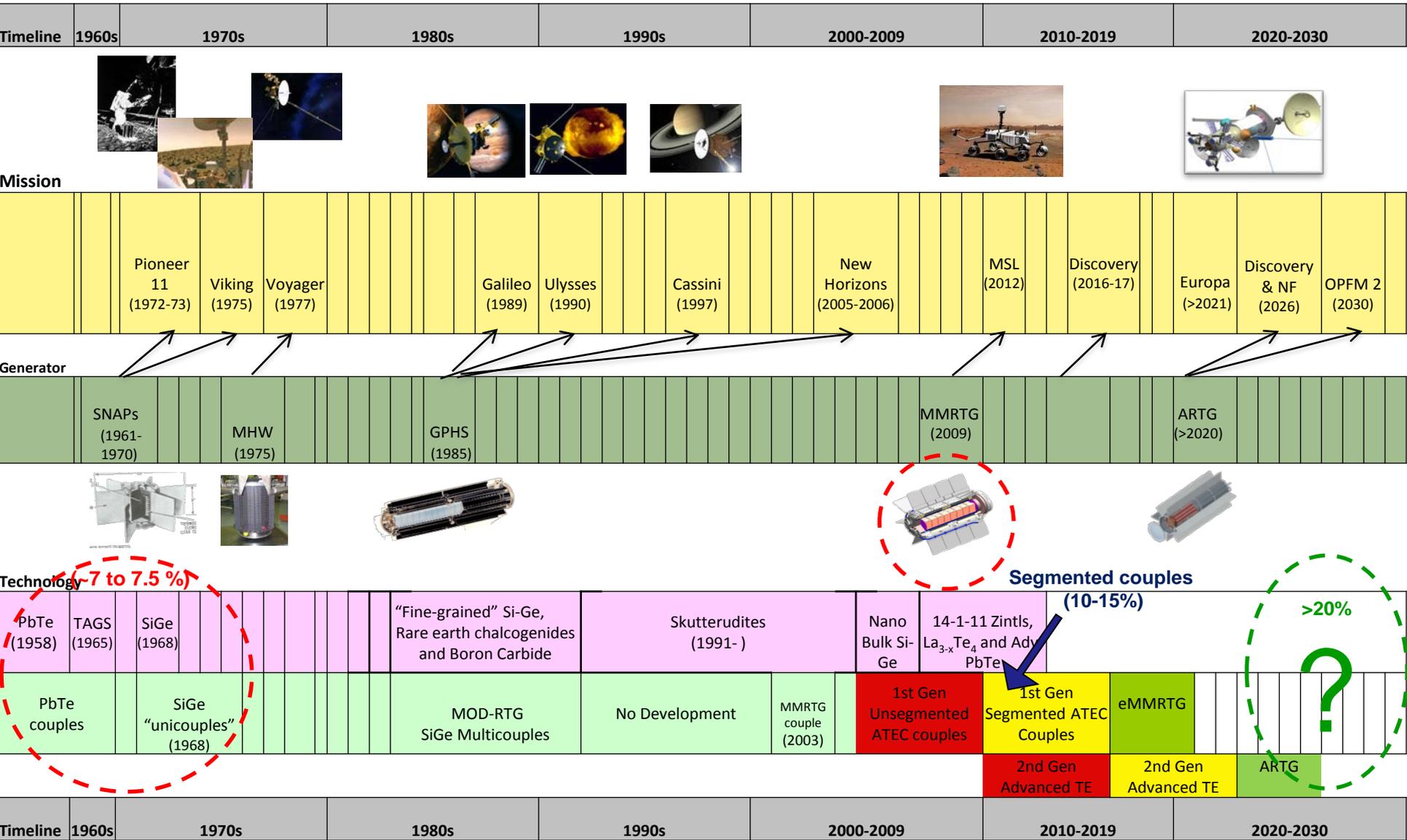
- For over 50 years, space nuclear power sources based on thermoelectric energy conversion have proved to be safe, reliable, sturdy, long-lived sources of electrical power.
- Since 1961, the U.S. has successfully launched 47 nuclear power sources (46 radioisotope thermoelectric generators and one nuclear reactor) on 28 space missions along with hundreds of radioisotope heater units (RHUs).
- The SNAP-10A space nuclear reactor power system demonstrated the viability of automatically controlled, liquid-metal-cooled reactors for space applications.
- RTGS have enabled some of the most challenging and scientifically exciting missions in human history
- In general, RTGs have exceeded their mission requirements by providing power at or above that required and beyond the planned mission lifetime.



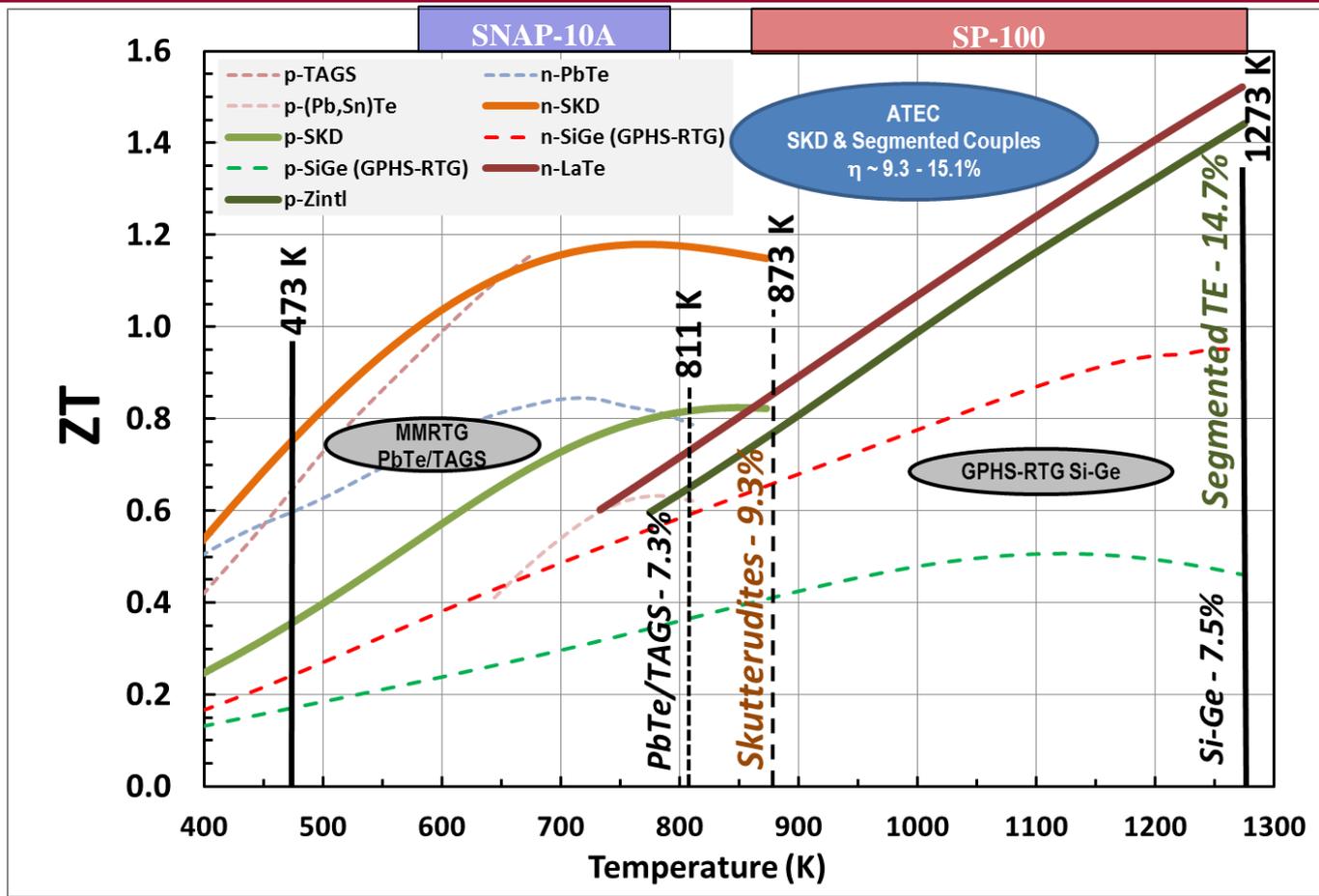
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# The Path Forward

# High Temperature TE Materials & RTG Technology Development Timeline



# Thermoelectric Materials and Device-Level Performance: x2 Increase over State-of-Practice May be Now Possible



**> 11% efficiency** projected for ARTG based on 1273 K/523 K operating temperature differential  
(GPHS-RTG: 6.5%)

**~ 8% efficiency** projected for eMMRTG based on 873 K/473 K operating temperature differential  
(MMRTG: 6.2%)

**~ 9% efficiency** projected for Small FPS based on 1060 K/505 K operating temperature differential  
(SP-100: 4.0%)

**x 2 increase in  $ZT_{ave}$  over SOA Si-Ge alloys (1275 to 475 K  $\Delta T$ ) when combined through segmentation**

$T_H/T_C$ (K)	1275 / 475	1075 / 475	975 / 475	875 / 475
Predicted TE Couple Efficiency	13.7%	11.2%	10.0%	9.3%
Demonstrated Efficiency (BOL)	14.8%	11.0%	10.0%	9.3%

# Potential Near Term Space & Terrestrial Applications for Advanced TE Power Systems



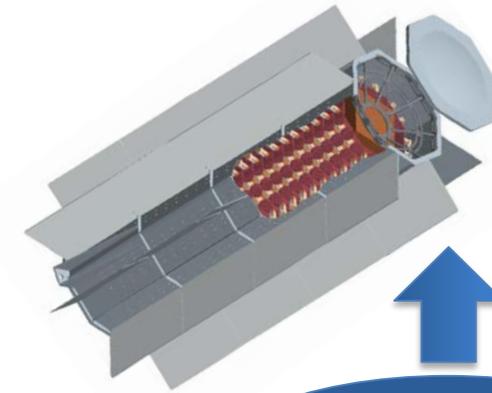
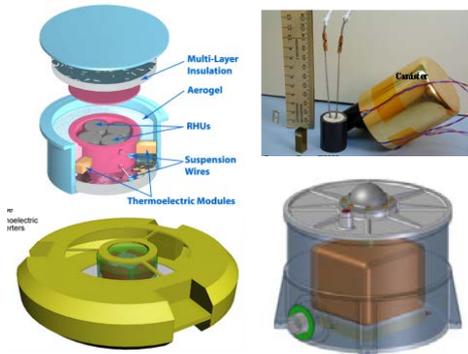
Early 2020's

## Enhanced MMRTG

- ~ 160 W
- ~ 3.8 W/kg
- ~ 8% efficiency

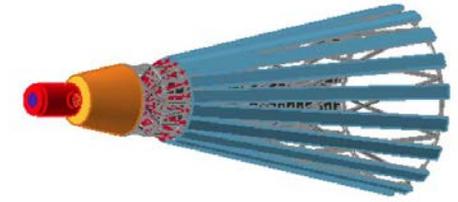
## Small RTGs

- 0.1 to 20 W



## Advanced RTGs

- 200-500 W
  - Up to 8.6 W/kg
  - > 11% efficiency
- Late 2020's

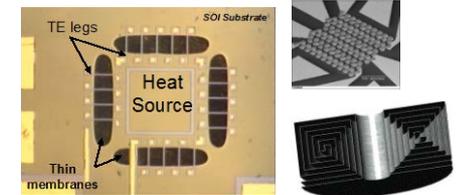


## Fission Reactor Power System

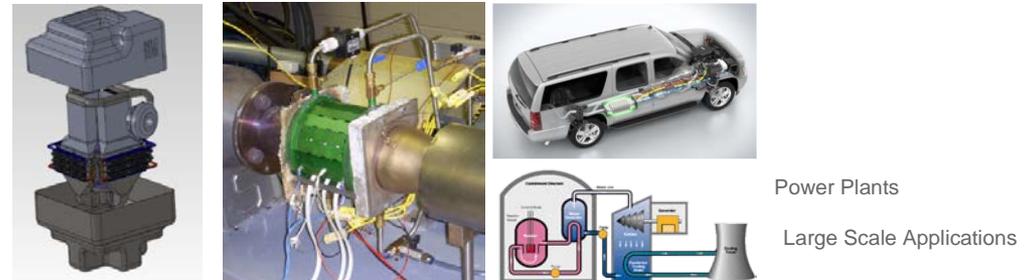
- 0.5 to 10's of kW-class

## Energy Harvesting

- Miniaturized devices
- Extreme environments



## Auxiliary and waste heat recovery power systems



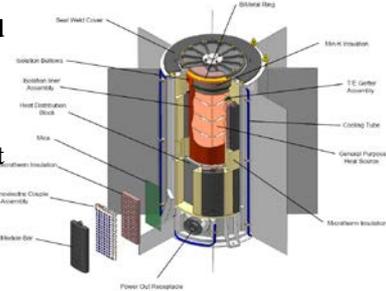
Power Plants  
Large Scale Applications

**Advanced high temperature TE technology being developed for space power systems could also be applied to terrestrial Waste Heat Recovery and auxiliary power systems**

# Power levels for Radioisotope Power Systems

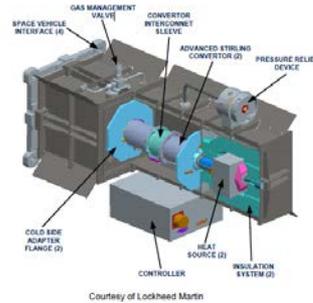
**MMRTG**  
Flight Qualified  
(on MSL)

**eMMRTG**  
In Development  
(~ 2022)

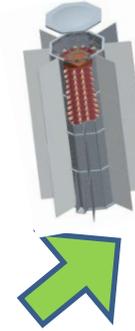


~ 120 to 160  $W_e$ , 6.3% to 8% eff., 44 kg  
~ 1880  $W_{th}$  at 450 K  $T_{rej}$

**ASRG**  
In development  
(~ 2028)



~ 140  $W_e$ , 28% eff., 32 kg  
~ 360  $W_{th}$  at 350 K  $T_{rej}$



**Advanced RTGs (~ 2030)**  
At TE couple development stage

> 11% system efficiency  
Potential for modular design  
(1 to 16 GPHS 250  $W_{th}$  blocks)  
~ 23 to 500  $W_e$   
~ up to 8.6  $W/kg$   
~ 500 K  $T_{rej}$

## Existing Flight Qualified Heat Sources



GPHS (250 Wt)

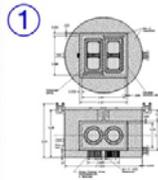


RHU (1 Wt)

## Application Power Levels

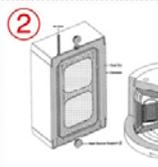
### >100 Watts

- Under development – MMRTG & SRG
- >110  $W_e$  & 35-40 kg per unit
- 2-8 GPHS per unit
- Available by 2008-2009



### 10 to 20 Watts

- Preliminary concept studies only
- 1 GPHS per unit
- Can use existing thermoelectric technology
- Requires systems engineering development



### 0.1 to < 10 Watts

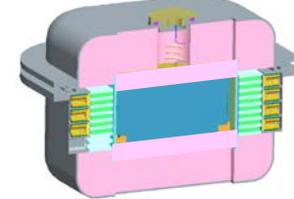
- Some concept studies from early 1990's
- Fractional GPHS or assembly of RHUs
- Requires **redesigned thermal source aeroshell** and systems engineering development
- **More extensive development than options 1 or 3**



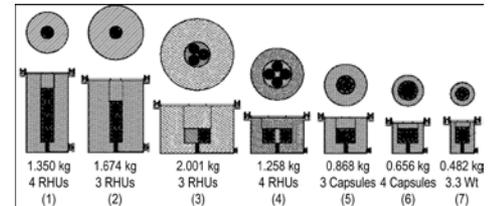
### ≥ 0.01 Watts

- Concept studies and technology development (Hi-Z)
- ≥1 RHU thermal source per unit
- Requires systems engineering development

**Small RPS (RTG and SRG)**  
Limited development



~ 20 to 50  $W_e$ , 6-10 kg  
~ 230 to 150  $W_{th}$  at 400-350 K  $T_{rej}$



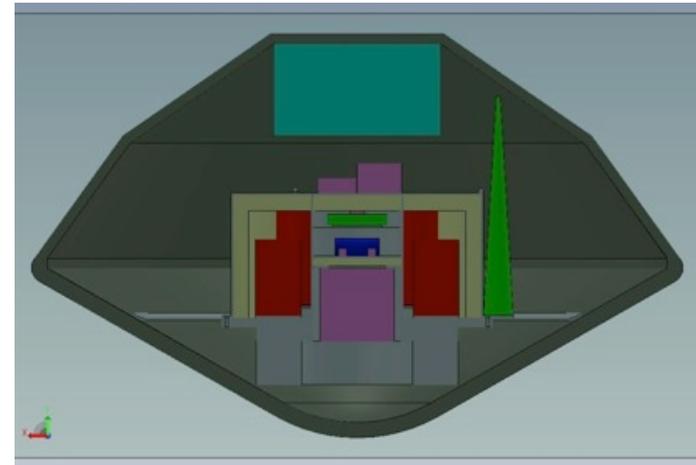
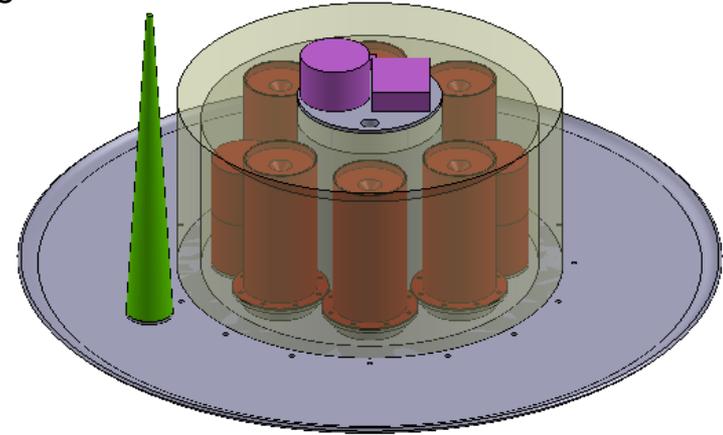
- 1.1  $W_{th}$  per RHU
- 4% efficient for 500 to 300 K operation
- ~ 45  $mW_e/RHU$
- But could be 6-10% efficient between 300 and 100 K (Carnot!)

Low Power (40 – 300 mW)

Radioisotope Thermoelectric Generators Concepts

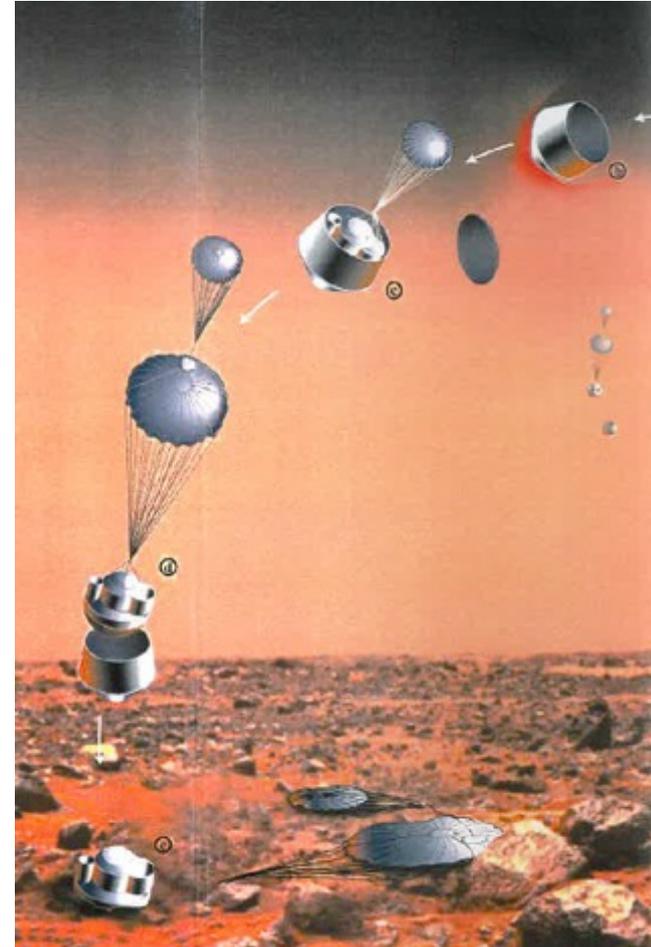
# Opportunities for Very Small RTGs

- Even at 40-250 mW of power, RHU-based very small RTGs could enable hard landers that house long duration sensors in challenging environments
  - Power/heat enables night-time operations
  - Power/heat enables polar winter operations
  - Power/heat simplifies in-space free flight (no solar arrays/batteries needed after carrier separation 1 Week before entry)
- The heat from the RHU-RTG, combined with capacitor systems and low temperature tolerable electronics ( $-40^{\circ}\text{C}$ ) are as important as the power output
- Due to the insulation required, the RHU-RTG power system dominates the interior volume of the lander
- RHU-based very small RTGs starting from 0.3 kg and 40 mWe
  - Single RHU-based concepts could use technology based on  $\text{Bi}_2\text{Te}_3$  materials : TRL is already at 5;
  - Multi-RHU concepts could use Skutterudites: TRL  $\sim 3$



# Potential Mission: Mars Sensor Network Concept

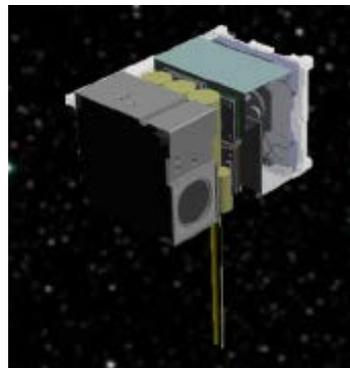
- Network of hard landers for a Mars Geophysical and Climate Network
- Long-life seismometry and climate monitoring enabled by RPS, RHU-RPS necessary to fit in Entry-Descent-Landing aeroshell
- Primary science objectives
  - Characterize the internal structure, thermal state, and meteorology of Mars.
- Targeted Measurements:
  - Temperature
  - Pressure
  - Seismometry
  - Optical (suspended dust and vapor)
  - Wind



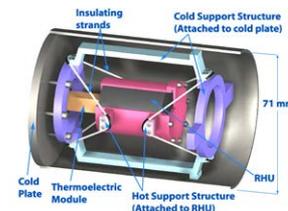
Pictured: Pascal hard lander

# mW RPS for CubeSats and Micro Instruments

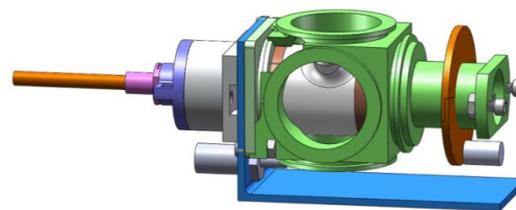
- Very small RTGs would enable CubeSats or micro instruments in support of long duration science and explorations missions.
  - Targeted Destinations
    - Mars – poles , craters, moons
    - Moon – shadowed craters, lunar night
    - Asteroids, Comets and other planetary moons
  - Targeted Micro Instruments
    - Surface (composition) or atmospheric (seismic or meteorological) measurement instruments



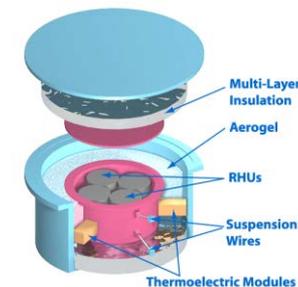
Notional S/C for MIRAGE Mission



1-RHU mW-RPS Prototype



Compact Vector Helium Magnetometer



4-RHU mW-RPS concept

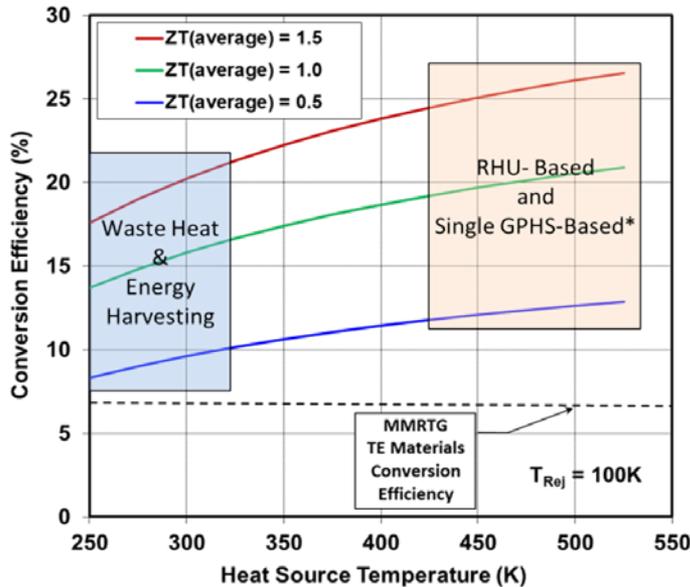
**Enable and Encourage New Creative and Innovative Mission and Instrument Concepts with mW RPS Option to Meet Low Cost Missions Power Demands for NASA's Future Missions.**

## “non-RPS” Options

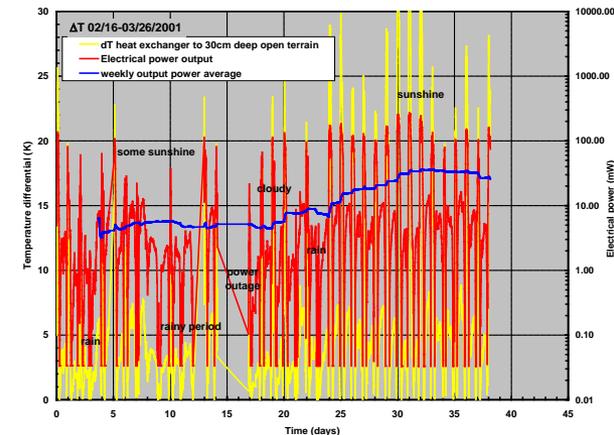
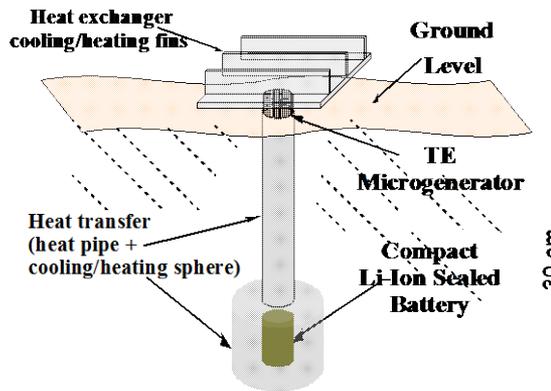
# Thermal Energy Harvesting

- High efficiency from high grade heat sources
    - Combustion/catalytic heat (Titan?)
    - Concept also applicable to fuel cells (ice)
  - Low efficiency from low grade heat sources
    - Waste heat from “hot” components
    - Energy harvesting from “natural” temperature differential
  - Could enable longer operation than just on primary batteries
    - Depends on required duty cycle – requires rechargeable energy storage component
    - Depends on thermal management requirements of other components and subsystems
    - Could be an intermediate, non-nuclear option of operation on icy moons
- Hybrid architecture possible (power tiles, power sticks...)

Technology	SOP	Performance Targets
Rechargeable batteries Supercapacitors	-30° C -40° C	-80° C -90° C
TE Generators	6.5% efficiency for >175° C heat sink	> 14% efficiency for heat sink > -20° C
Integrated Power System	> -55° C	-120° C



## JPL demonstration of In-Ground Thermoelectric Energy Harvester for distributed sensor networks



# Example: Titan In-Situ Energy Generator Options

- First step is to capture thermal energy from atmospheric entry
  - Integrate entry vehicle surface with heat pipe
  - Transfer thermal energy from entry vehicle surface to thermal energy storage material
  - Capture thermal energy at capacity of thermal energy storage device
- Second step is to transfer thermal energy to system 'start up' phase
- Third step is to proceed through generator 'start up' sequence to reach steady state operation using catalytic combustor
  - Lander has stored oxygen (LOX) onboard (25 L -> 100 kWh thermal energy)
  - Assumes hydrocarbons on Titan are readily available to lander
- Fourth step is to charge the onboard secondary battery
- Fifth step is to synchronize the generator/battery state-of-charge/energy duty cycle for optimized use of stored oxygen

# Example: PV/Battery Power Sheet Technology

## MAIN CONCEPT:

Integrated modular hybrid power system that contains:

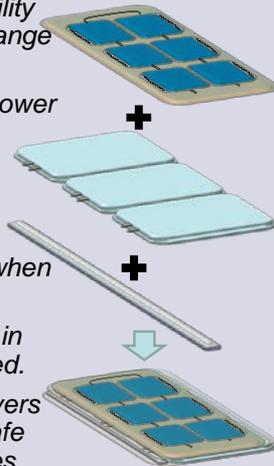
- Power generation system - highly efficient, low cost ultra-thin photovoltaic cells (> 30% solar conversion efficiency)
- Energy storage system - high energy density rechargeable batteries (>250 Wh/kg) with fast charging capability and wide operating temperature range
- Power management system - integrated charge electronics for power regulation and distribution

## HOW IT WORKS:

- Solar arrays charges the battery when sunlight is available
- Battery delivers power to loads in nighttime and daytime as needed.
- Power management system delivers power at 15/30 volts, insures safe recharging of batteries, provides energy metering capability and load management

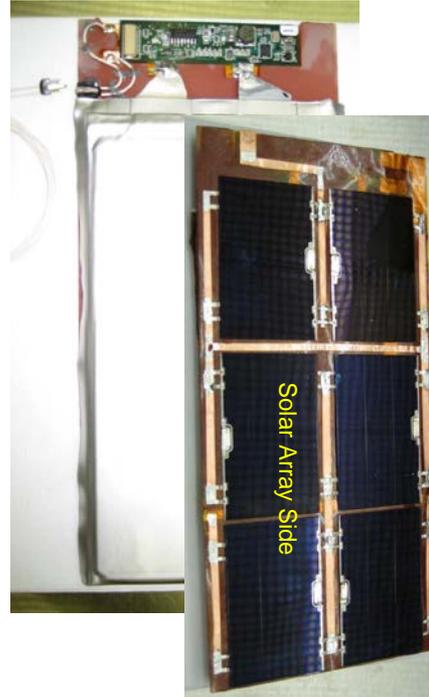
## ASSUMPTIONS AND LIMITATIONS:

- Availability of solar energy
- Availability of in-field charge time during mission



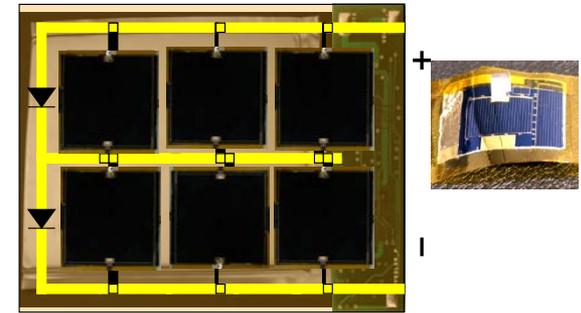
## 32 Wh Power Sheet Demo (Single Module Built and tested)

Uses Dual Junction thick solar cells and Li-Ion polymer pouch cells



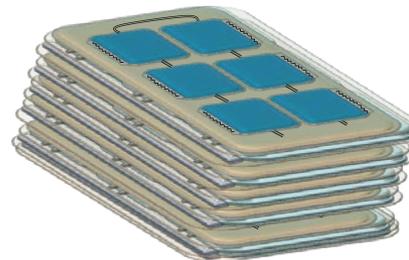
## 6 Wh Power Sheet Demo (Module Components tested)

Uses Triple Junction ultrathin solar cells and Li-Ion polymer pouch cells

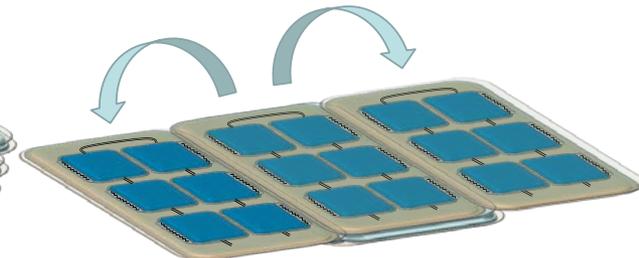


## 720 Wh POP Target (Projected Performance)

Uses > 30% efficient ultrathin solar cells and 300 Wh/kg rechargeable pouch cells



**720 Wh**  
**24-Module Stack Stowed**  
(less than 2 liters and 4 kg)



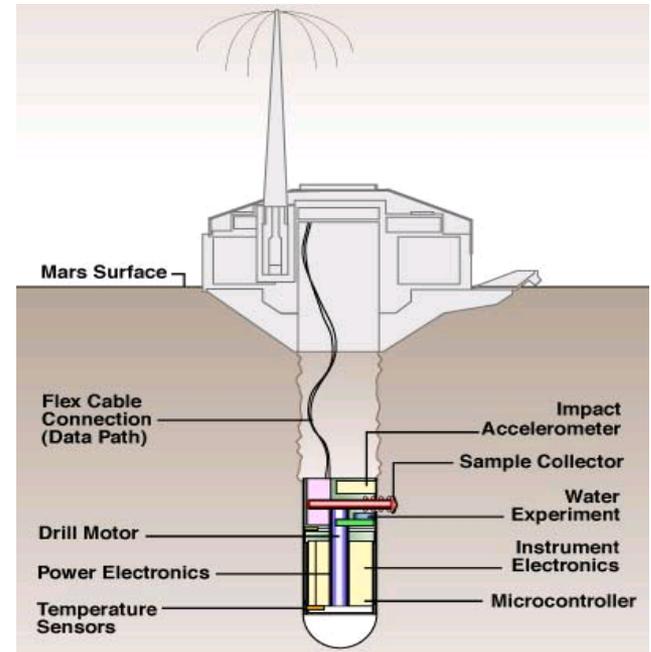
**30 Wh Single Module Deployment**  
**of extra Ultrathin Solar Array "flaps"**

# Low Temperature Lithium Primary Batteries

## Background: Mars DS2 Microprobe Spacecraft



- Launched on January 1999
- Two microprobes (2.4kg) piggybacked on Mars Polar Lander mission
- Intended as a low cost, high risk/high payoff mission
- Design:
  - No parachute: dropoff penetrator
  - Aftbody with batteries & telecom stays on surface
  - Forebody penetrates, ~ 1 meter
  - Drill scoops soil sample into chamber
  - Heat, vaporize, and analyze for H<sub>2</sub>O
  - Transmit water and other science data



*DS2 spacecraft*



# Battery technology development options

Development time frame	Energy Density	Estimated discharge temperature limits	Issues
Short term	~60 Wh/kg	-60°C at C/20	Charging <-40°C
	~40 Wh/kg	-60°C at C/5	Charging <-40°C
	~40 Wh/kg	-70°C at C/50	Charging <-40°C
Mid term	~200 Wh/kg (projected)	?	Charging <-40°C
Long term	200-250 Wh/kg	-130°C to -145°C	Primary battery, low TRL