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# **Large Space Apertures: Kick-off Workshop**


## **State of the Art: Active and Adaptive Optics**

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**November 10, 2008**

# Acknowledgement

- This paper was first presented at the 2008 SPIE Astronomical Instruments Symposium, Marseille, France:

 National Aeronautics and Space  
Administration  
Jet Propulsion Laboratory  
California Institute of Technology

## Active Optics for a 16-Meter Advanced Technology Large Aperture Space Telescope (ATLAS-T16)

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# ATLAST Study Goal: ID Tech Needs

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- **The Ares-V cargo launch vehicle offers the possibility of a truly large space telescope in the 2020 time-frame**
  - 8.8 m diameter by 18.7 m long shroud
  - 55,600 kg to L2 orbit
- **ATLAST Study objective is to create a technology plan leading to development of a new flagship mission for NASA**
  - Study team led by ST ScI (Marc Postman), with participation from 4 NASA Centers, 4 Universities, and 2 system contractors (Ball and NG)
- **Two concepts are being pursued:**
  - 16 m aperture, deployed telescope with a segmented Primary Mirror (PM)
  - 8 m aperture, monolithic, non-deployed telescope (H.P. Stahl, this meeting)
- **This paper considers the special technical challenges of the 16-m system**

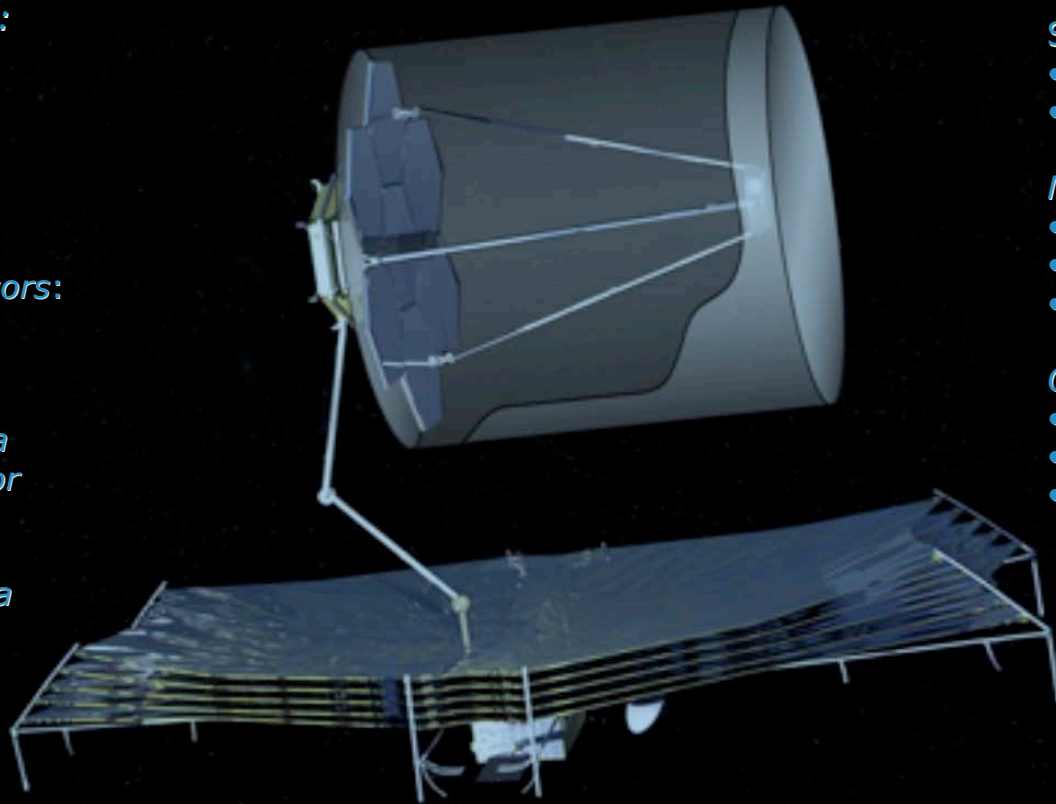
# WF Sensing and Control Baseline

## Optics and optical controls:

- Segmented primary
  - Deforming actuators
  - Rigid-Body actuators
- Deployed secondary
  - Rigid-Body actuators

## Instruments and WF sensors:

- High-dynamic range imager
- Visible imager
  - Phase Retrieval Camera
  - Dispersed-Fringe Sensor
- Spectrometer
- UV imager
- Shack-Hartmann Camera



## Spacecraft System:

- Attitude Control
- Command and telemetry

## Metrology System:

- Laser Truss
- Edge sensors?
- IRU

## On-board processor:

- Optical State Estimator
- WF Controller
- Pointing Controller

- Wavefront Sensing uses Imaging and Shack-Hartmann cameras and Laser Metrology to measure WF errors
- Wavefront Control uses the deformable/moveable PM segments to keep WF error small for diffraction limited image quality
- Line-of-Sight Pointing Sensing and Control will use a Fast Steering Mirror driven from Metrology and/or Guide Star error signals to limit jitter



# ROM Wavefront Control Requirements

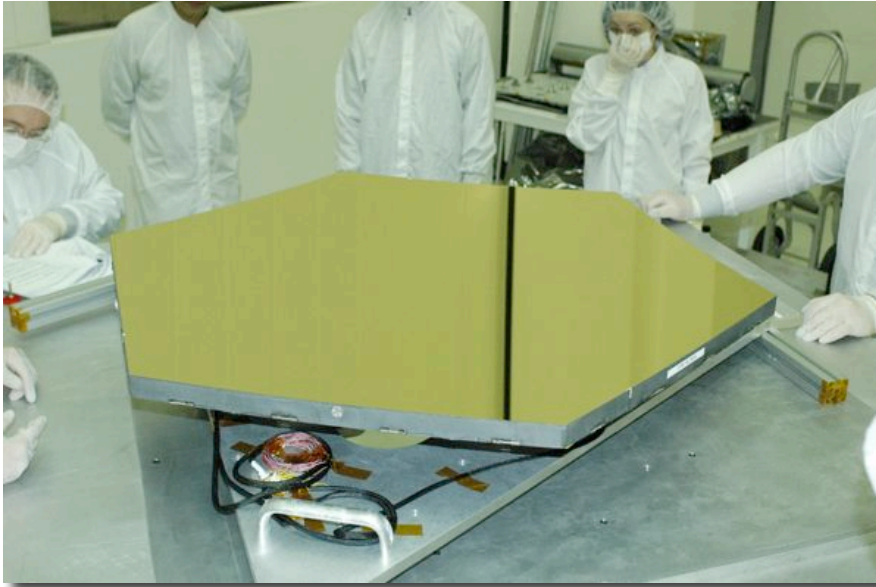
- Exoplanet imaging is perhaps the most demanding task for an ATLAS-T16 telescope
- WF performance required will depend on implementation
  - Does the Planet Imaging (PI) instrument provide a second layer of control?
  - Is an external occulter to be used?

	No PF instrument	No WFC in PF instrument	Second stage of WFC in PI instrument	High BW WFC in PI instrument	External occulter	External occulter + moderate coronagraph
WF Error	10-40 nm	<1 nm	10-40 nm	10-40 nm	10-40 nm	10-40 nm
WF Stability	5-20 nm	<1 nm	<1 nm	5-20 nm	5-20 nm	1 nm

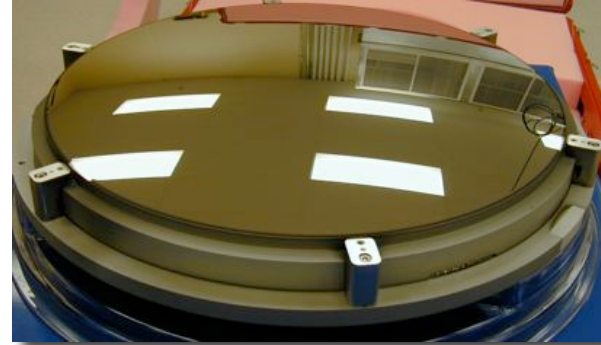
- LOS pointing performance for PI is similarly extreme

- Target telescope WF performance for good general astrophysics performance
  - Use a PI instrument with active WFC, or with an external occulter
    - Telescope static WFE < 10-40 nm RMS
    - Telescope WFE stability < 5-20 nm RMS

# Lightweight Active Optics



- ATLAST-16 will require lightweight, actively controlled optics such as Active Hybrid Mirrors (AHMs)
- AHMs combine a cast SiC substrate with integrated ceramic actuators, with a Nanolaminate facesheet



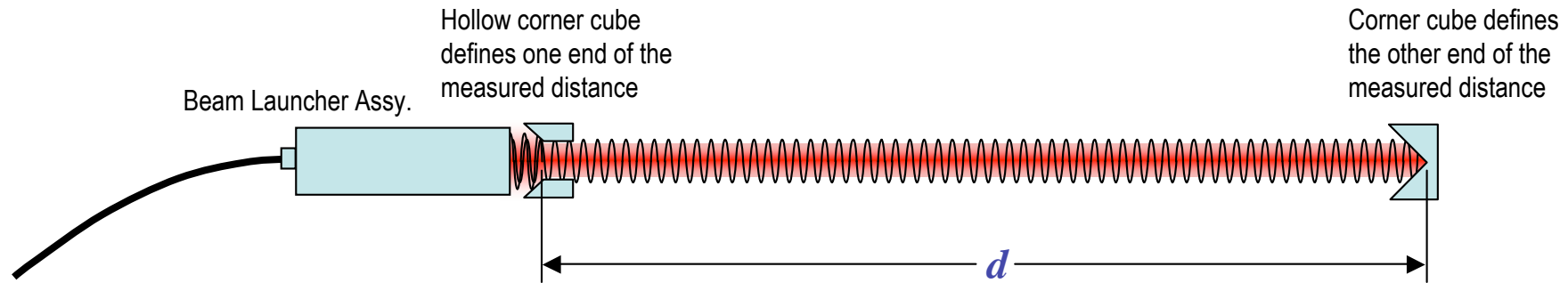
- Nanolaminate facesheet is a multi-layer metallic foil grown by sputter deposition on a precision mandrel
- AHMs are fabricated by replication for minimum cost and manufacturing time
- AHM technologies are a joint development of NG Xinetics, LLNL and JPL

# WF Control and Metrology Baseline

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- **Initial WF Sensing and Control establishes the metrology set-point**
  - Star observations for WFS&C during commissioning, and 1/day after that
    - Full-spectrum for segment phasing
    - Full field for Telescope alignment
- **Segment thermal control keeps segment figure constant**
- **Metrology keeps alignments constant, compensating for thermal deformation of the supporting structures**
- **Metrology technology options:**
  - Laser Truss     *Provides full observability of Telescope alignment errors*
  - Edge / Gap Sensors
  - Full-time WF sensing

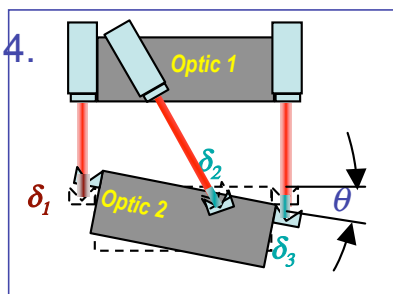
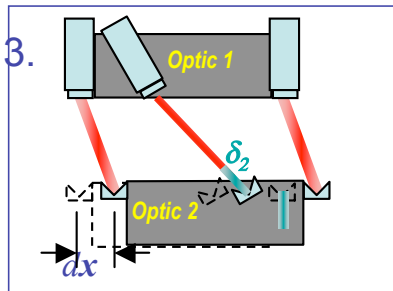
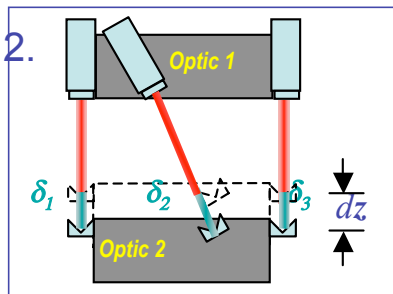
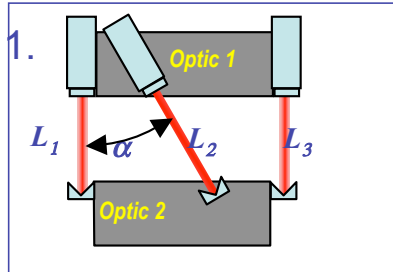
# A Laser Distance Gauge



- At the conceptual level, a Laser Distance Gauge (LDG) is a “yardstick,” with “inchmarks” provided by the interference fringes of the laser beam
  - Changes in the distance  $d$  between the Beam Launcher (BL) and the Corner Cube (CC) are measured as phase shifts between input and output beams
    - Intrinsic accuracy is better than 1 nm
    - We “count fringes” to track large changes in  $d$
    - A 2-color mode provides a large “absolute mode”
- We can keep the BL and CC the same distance apart, by position feedback control of the BL and/or CC to keep  $d$  constant
  - LDG runs at high BW (nominally 1 kHz)

▪ A SIM Mission-derived technology application funded by JPL R&TD

# A 2-Dimensional LT Example



- This 2-D example illustrates use of LDG measurements to estimate rotational as well as translational DOFs between bodies

1. Nominal geometry. There are 3 relative DOFs –  $x$  and  $z$  translation, and  $\theta$  rotation

2. Changes in LDG measurements due to a  $z$  translation:

$$\delta_1 = dz; \quad \delta_2 = \cos(\alpha)dz; \quad \delta_3 = dz;$$

3. Changes in LDG measurements due to an  $x$  translation:

$$\delta_1 = 0; \quad \delta_2 = \sin(\alpha)dx; \quad \delta_3 = 0;$$

4. Changes in LDG measurements due to a  $\theta$  rotation:

$$\delta_1 = r_1\theta; \quad \delta_2 = r_2\sin(\alpha)\theta; \quad \delta_3 = r_3\theta;$$

- The measurement in matrix form

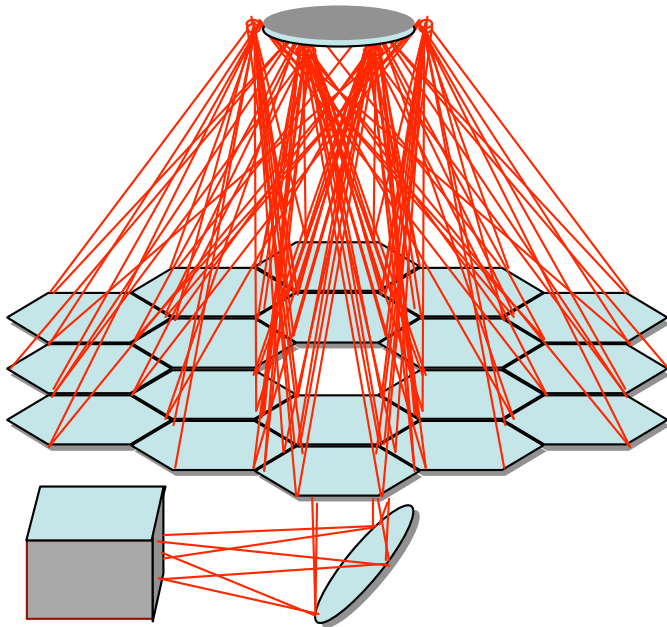
$$\delta = \begin{bmatrix} \delta_1 \\ \delta_2 \\ \delta_3 \end{bmatrix} = \begin{bmatrix} 0 & 1 & r_1 \\ \sin(\alpha) & \cos(\alpha) & r_2 \sin(\alpha) \\ 0 & 1 & r_3 \end{bmatrix} \begin{bmatrix} dx \\ dz \\ \theta \end{bmatrix} = Cx$$

- A simple state estimator

$$\hat{x} = C^{-1}\delta$$

- Feedback control based on the  $\delta$  measurements can keep the truss aligned

# The Full 3-Dimensional Laser Truss



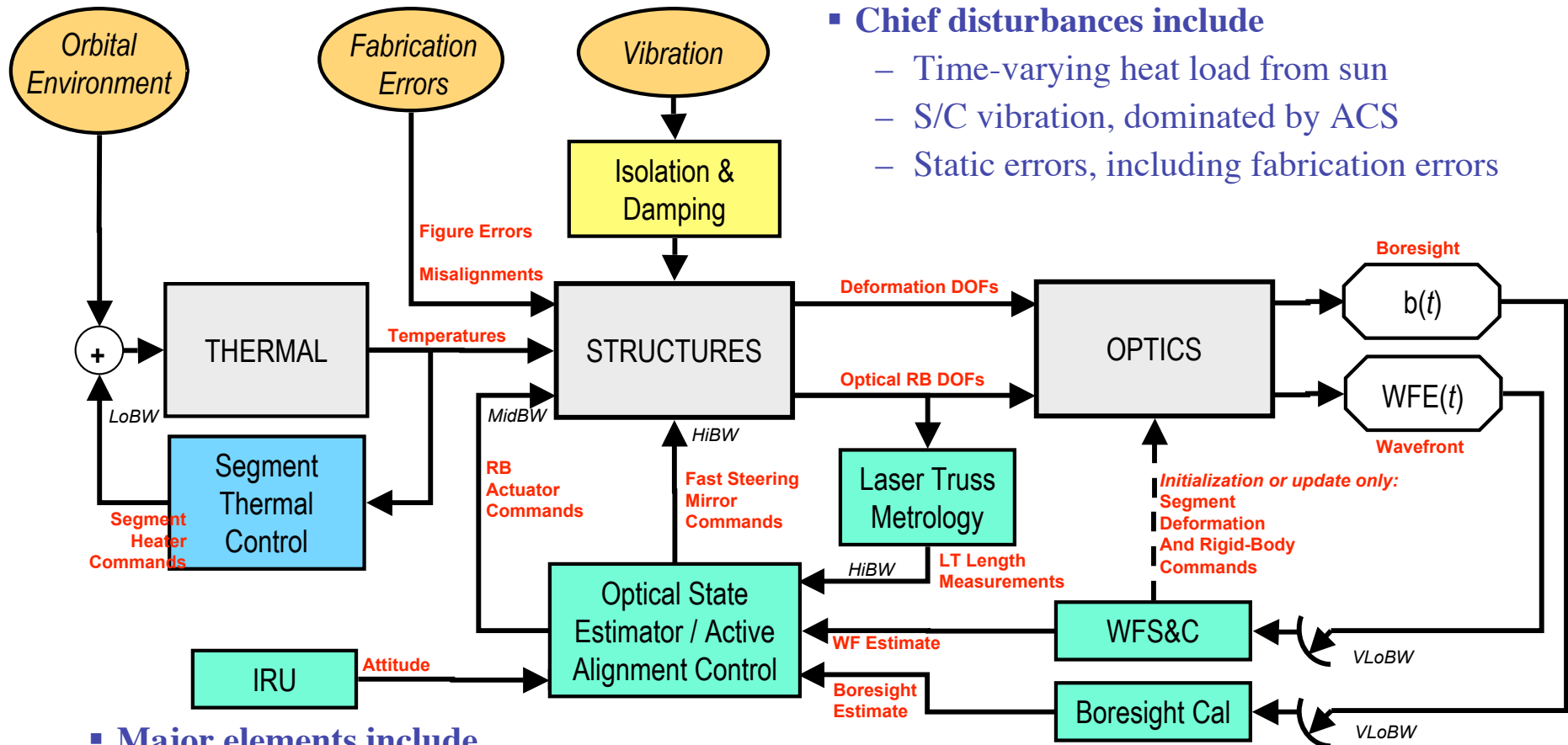
- The same approach is extended for the full 3-D LT
  - 6 LDGs per segment measure all relative RB DOFs in the entire OTA
    - All PM segments, the SM, FF, TM and OBA
  - The IRS is attached to the OBA, providing measurements of 6 more absolute DOFs wrt inertial space
- Same measurement equation:  $\delta = Cx$ 
  - Sensitivities computed from model kinematics

- Measurement is invertible:  $x = C^{-1}\delta$  is full rank
- *Optical State Estimator* uses a Kalman Filter to estimate the RB state
  - Balances measurement vs. prior knowledge for optimal estimate
  - Predicts WF and Boresight from state estimate
- Feedback control using RB actuators and optimal control laws keeps performance in spec
  - Integrated model will be used to evaluate performance

# Block Diagram

## Chief disturbances include

- Time-varying heat load from sun
- S/C vibration, dominated by ACS
- Static errors, including fabrication errors



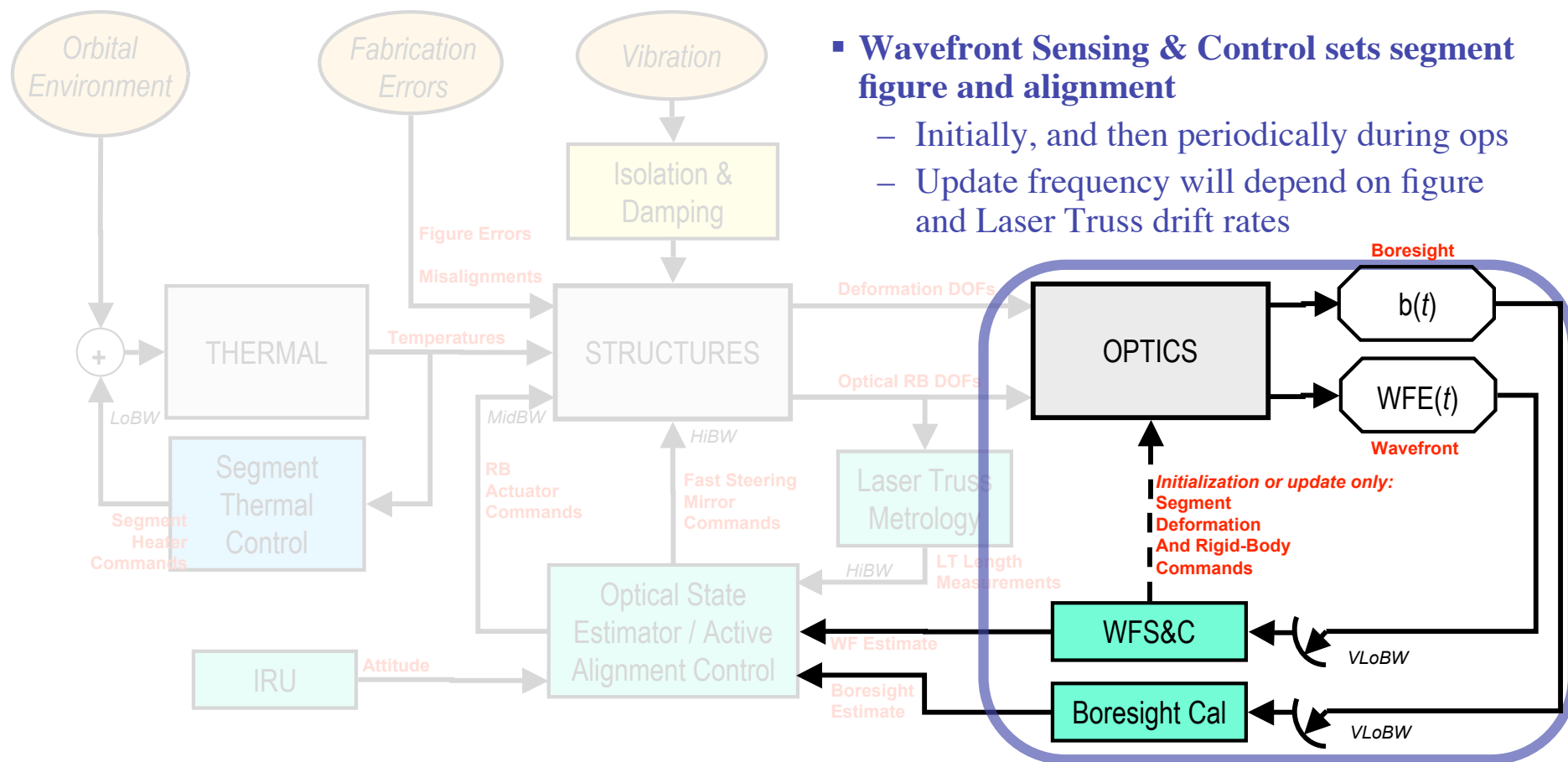
## Major elements include

- Wavefront Sensing and Control
- Laser Truss Active Alignment: active WF compensation and LOS pointing control
- Segment Thermal Control to stabilize optical figure
- Isolation and Damping to attenuate vibration disturbances

# Initial WFS&C

## Wavefront Sensing & Control sets segment figure and alignment

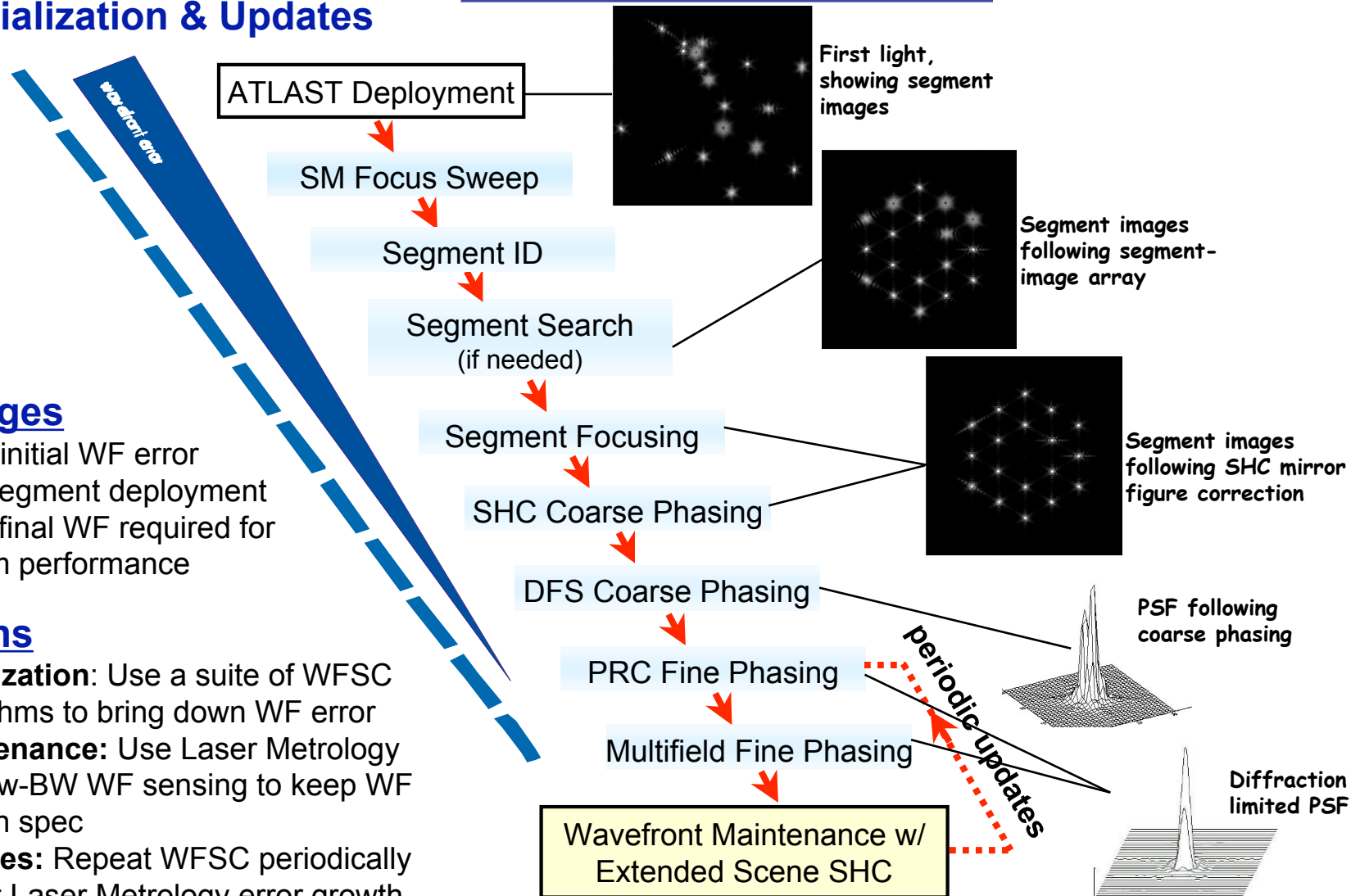
- Initially, and then periodically during ops
- Update frequency will depend on figure and Laser Truss drift rates



# WF Sensing and Control

Chart borrowed from JWST – Scott Acton/Ball

## WF Initialization & Updates



## WF Maintenance

### Challenges

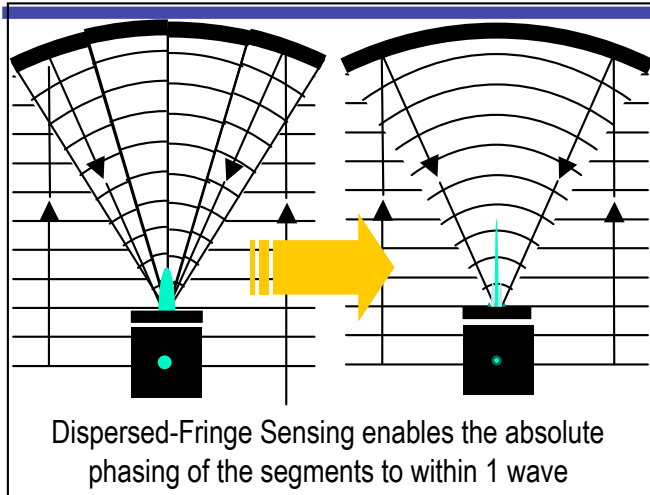
- Large initial WF error after segment deployment
- Small final WF required for system performance

### Solutions

- **Initialization:** Use a suite of WFSC algorithms to bring down WF error
- **Maintenance:** Use Laser Metrology and low-BW WF sensing to keep WF error in spec
- **Updates:** Repeat WFSC periodically to limit Laser Metrology error growth

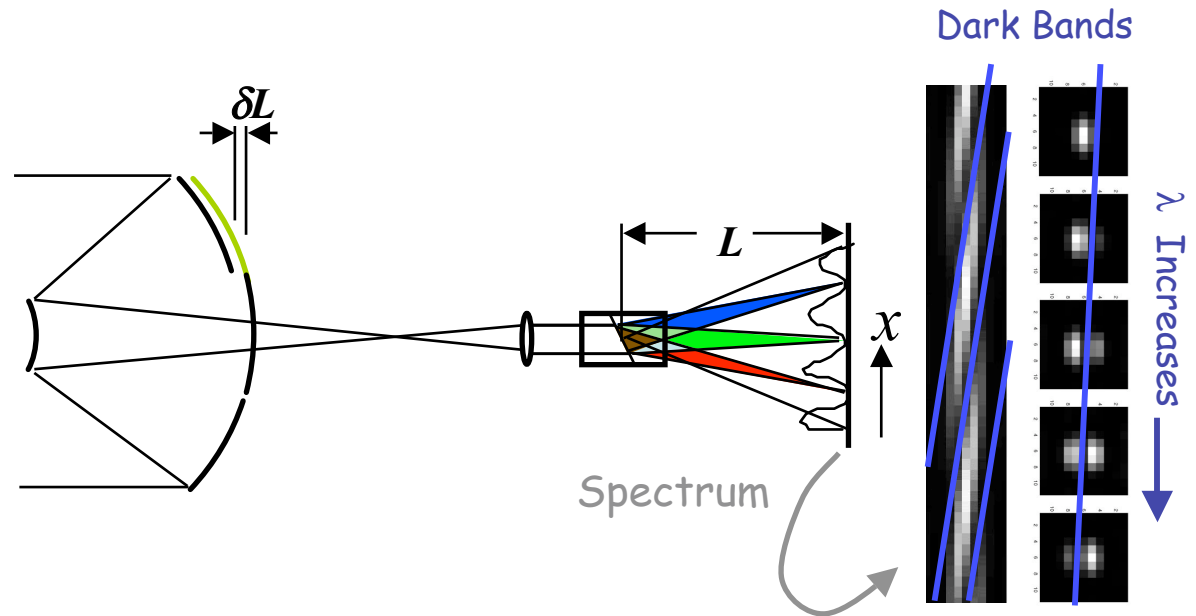


# Coarse Phasing: Dispersed Fringe Sensing



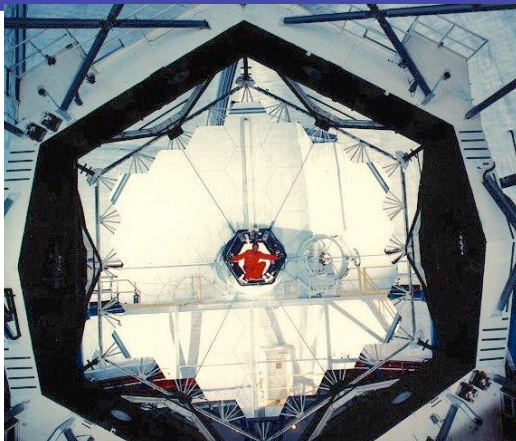
- DFS uses segment steering to select segment combinations for control
- “Dispersed Hartmann Sensing” (DHS) is DFS with prisms that select edge patches only
  - JWST approach

- Dispersed-Fringe Sensing (DFS) uses a dispersive element (a grism) in an imaging camera to spread spot images into linear spectra



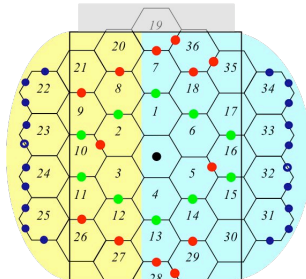
- Wavelength variation along the spectrum modulates fixed path differences between segments to create interference fringes:
  - Bright peak where  $\lambda$  is coherent with  $\delta L$
  - Dark null where  $\lambda$  is out of phase with  $\delta L$
- Period of fringe gives absolute piston displacement
- Slope of dark bands gives the sign

# Example: Keck DFS Experiment 2

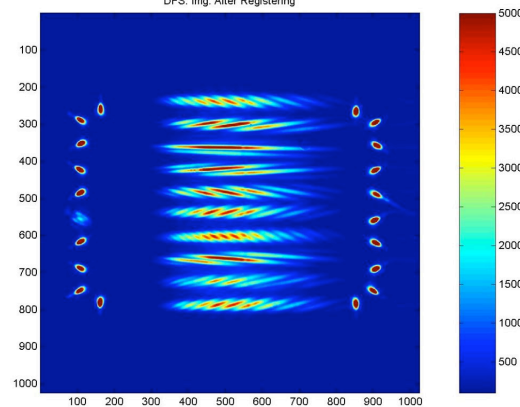


- Two DHS devices were used in the second Keck experiment
  - 0° and 60° grism orientations
  - 10 edges sampled in each image
- Combination provides enough information to reconstruct piston of 18 segments
  - Tilts constrained

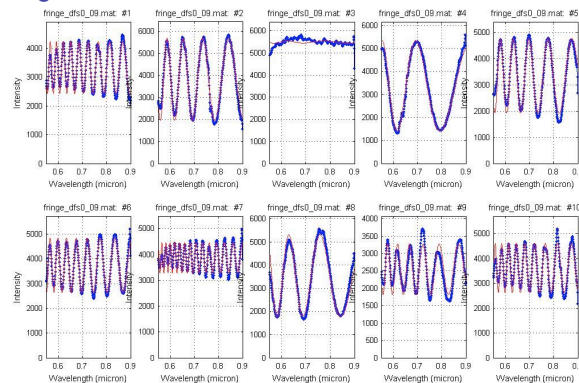
Sampling for 0° Device



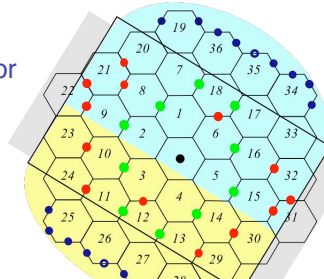
Fringe Image from 0° Device



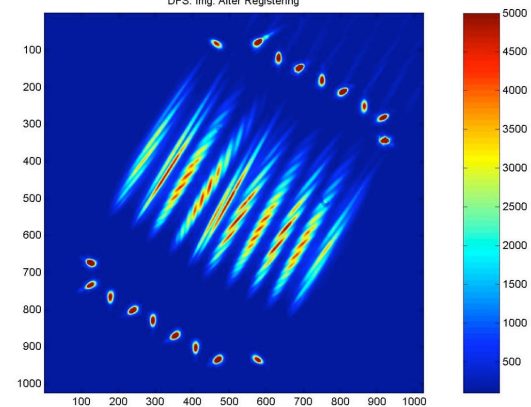
Signals and Fit from 0° Device



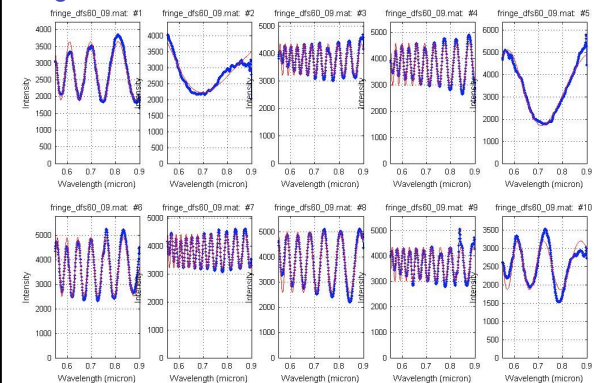
Sampling for 60° Device



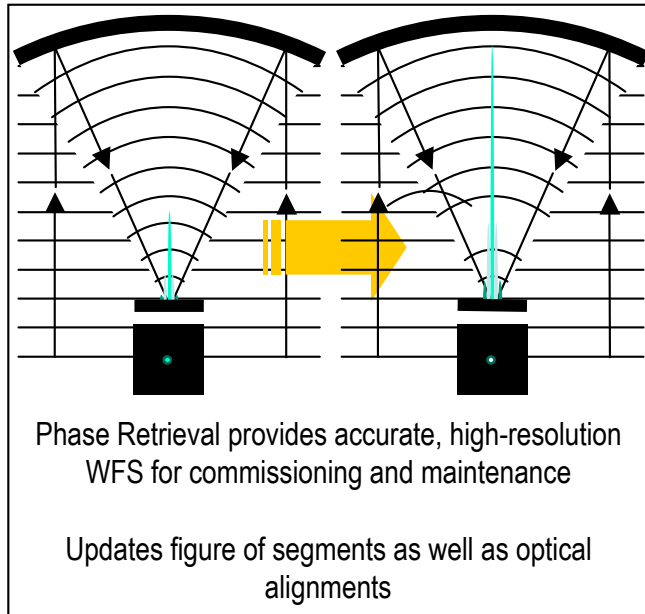
Fringe Image from 60° Device



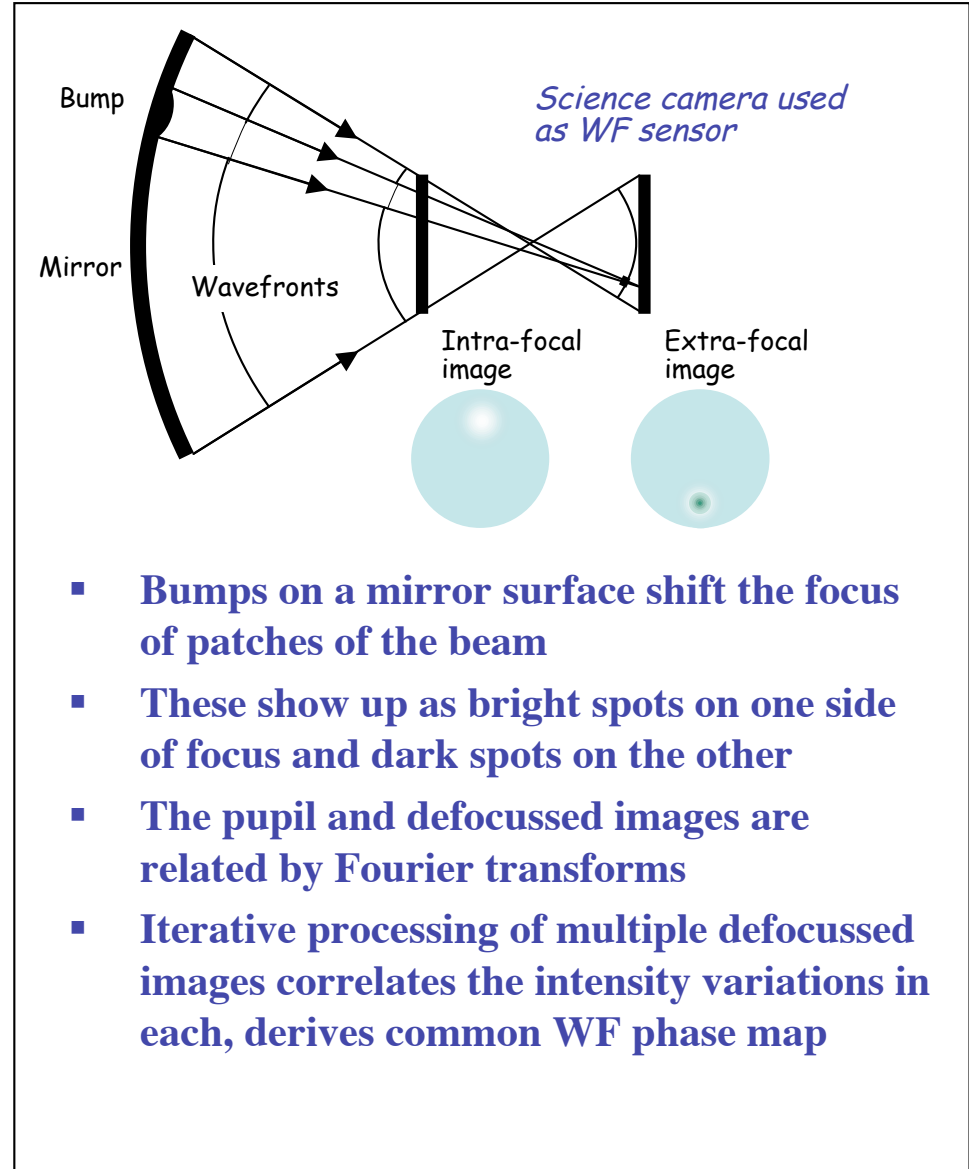
Signals and Fit from 60° Device



# Phase Retrieval WFS

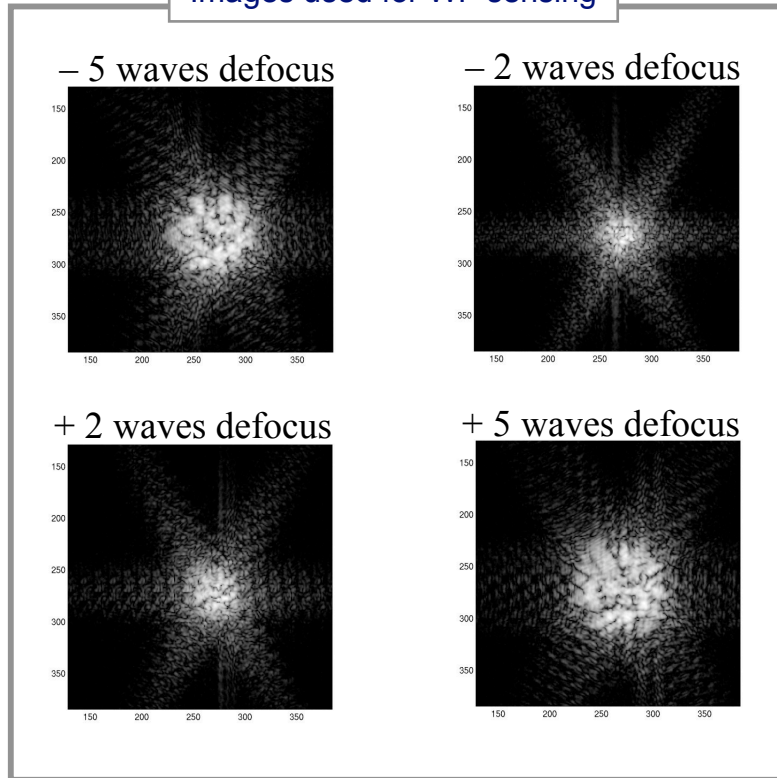


- **Image-based Phase Retrieval WFS offers**
  - High accuracy
  - High resolution
  - Can be performed in any camera, any field point
  - Minimum of non-common optics

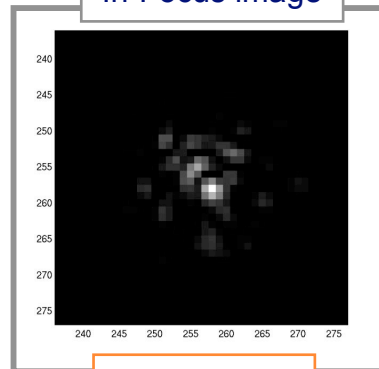


## Example: Fine-Phasing 36-Hex PM

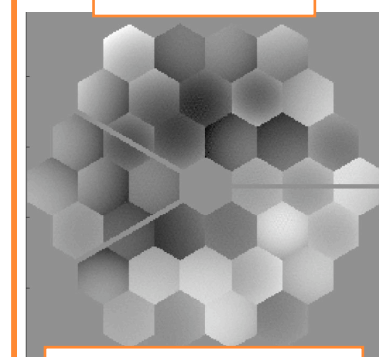
Images used for WF sensing



In-Focus image



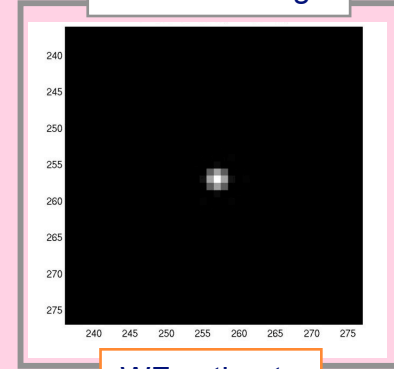
WF estimate



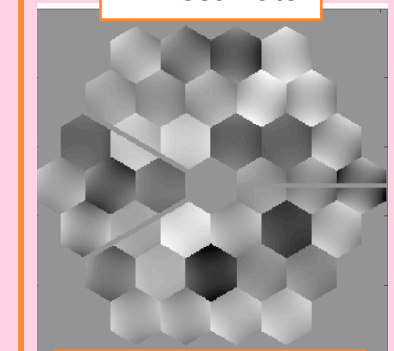
WFE=480 nm RMS

- Post-control WF meets 150 nm objective

In-Focus image



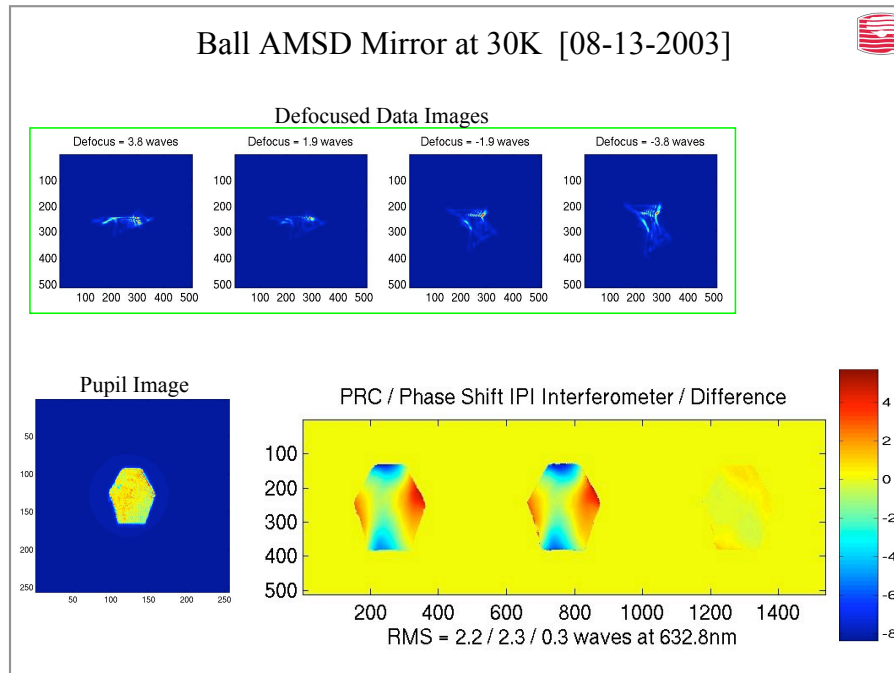
WF estimate



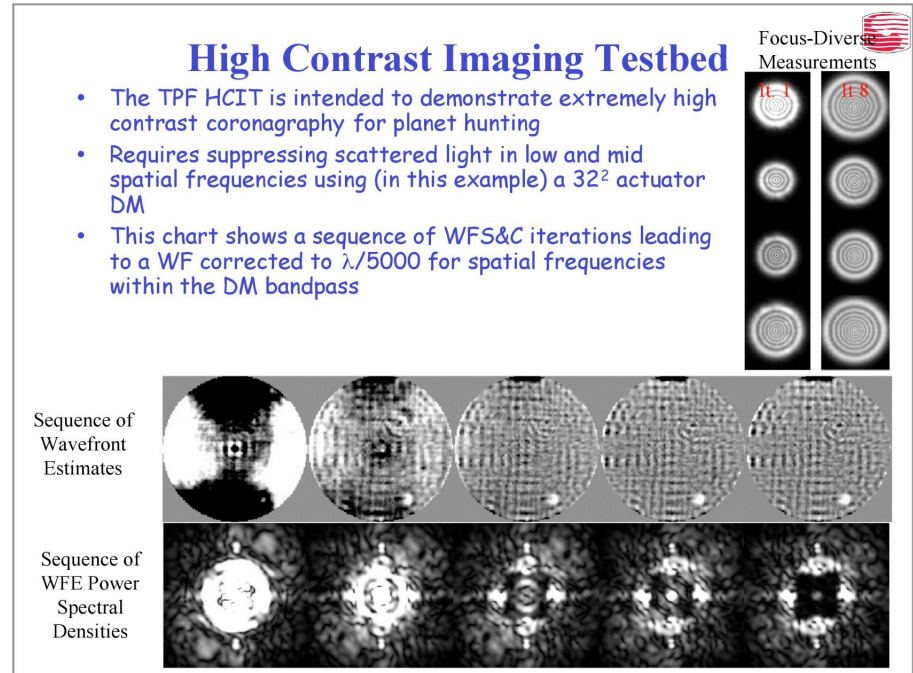
WFE= 35 nm RMS

- Fine Phasing uses MGS Phase Retrieval to estimate WF
- WF control is applied using segment RB and RoC actuators

# WFS Capture Range and Accuracy



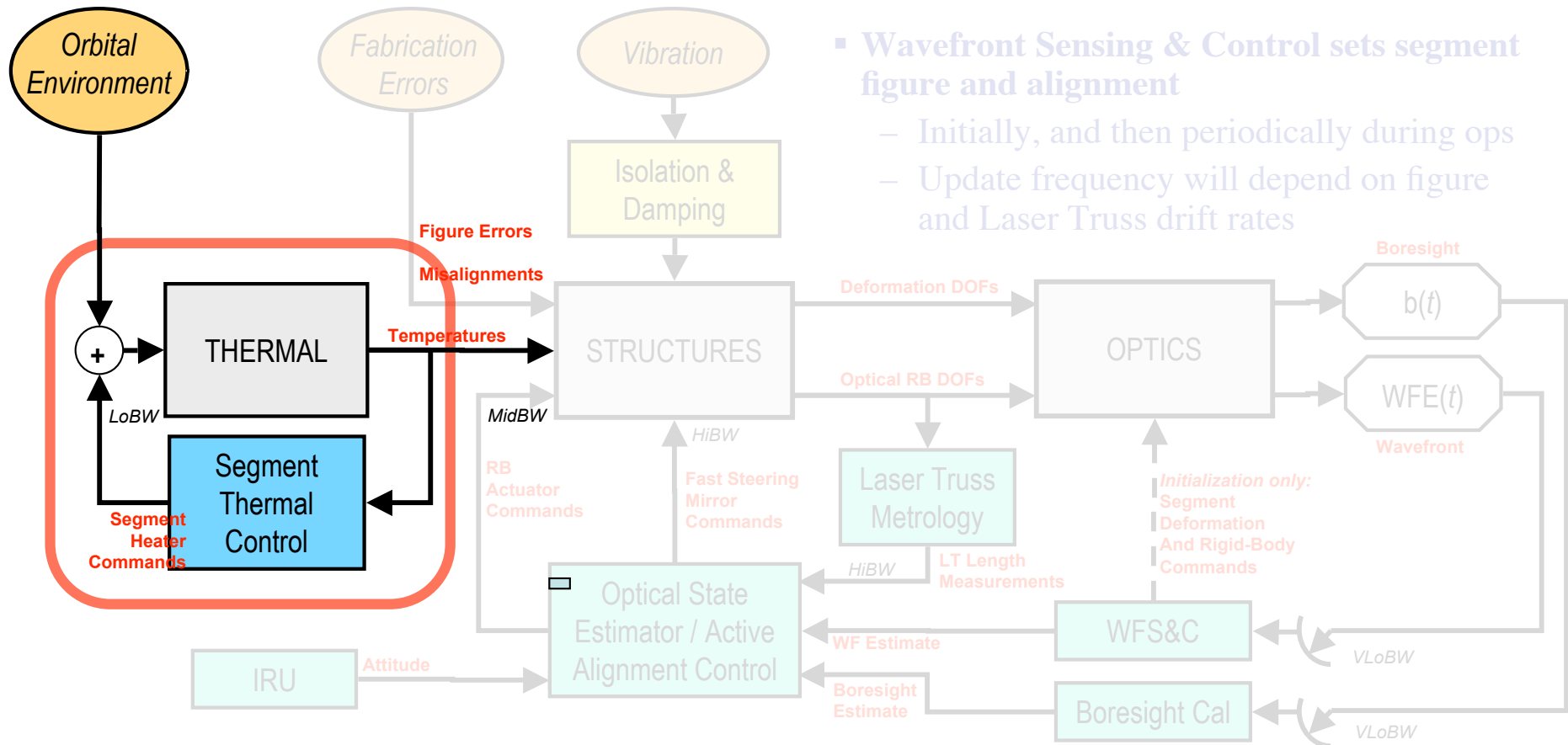
- PRC was used to test the 1.3 m-class Advanced Mirror System Demonstrator (AMSD) beryllium mirror, built by Ball Aerospace and tested at the MSFC XRCF facility
- Demonstrated >12 waves capture range, with < 8 waves of focus diversity



- JPL's High Contrast Imaging Testbed provides a highly stable test environment for WFS&C and Coronagraphy
  - Demonstrated  $\lambda/5,000$  WFS&C performance
  - Demonstrated  $6.4 \times 10^{-10}$  contrast at the 4<sup>th</sup> Airy ring, and 10% bandwidth centered at 800 nm



# Thermal Control Preserves PM Figure

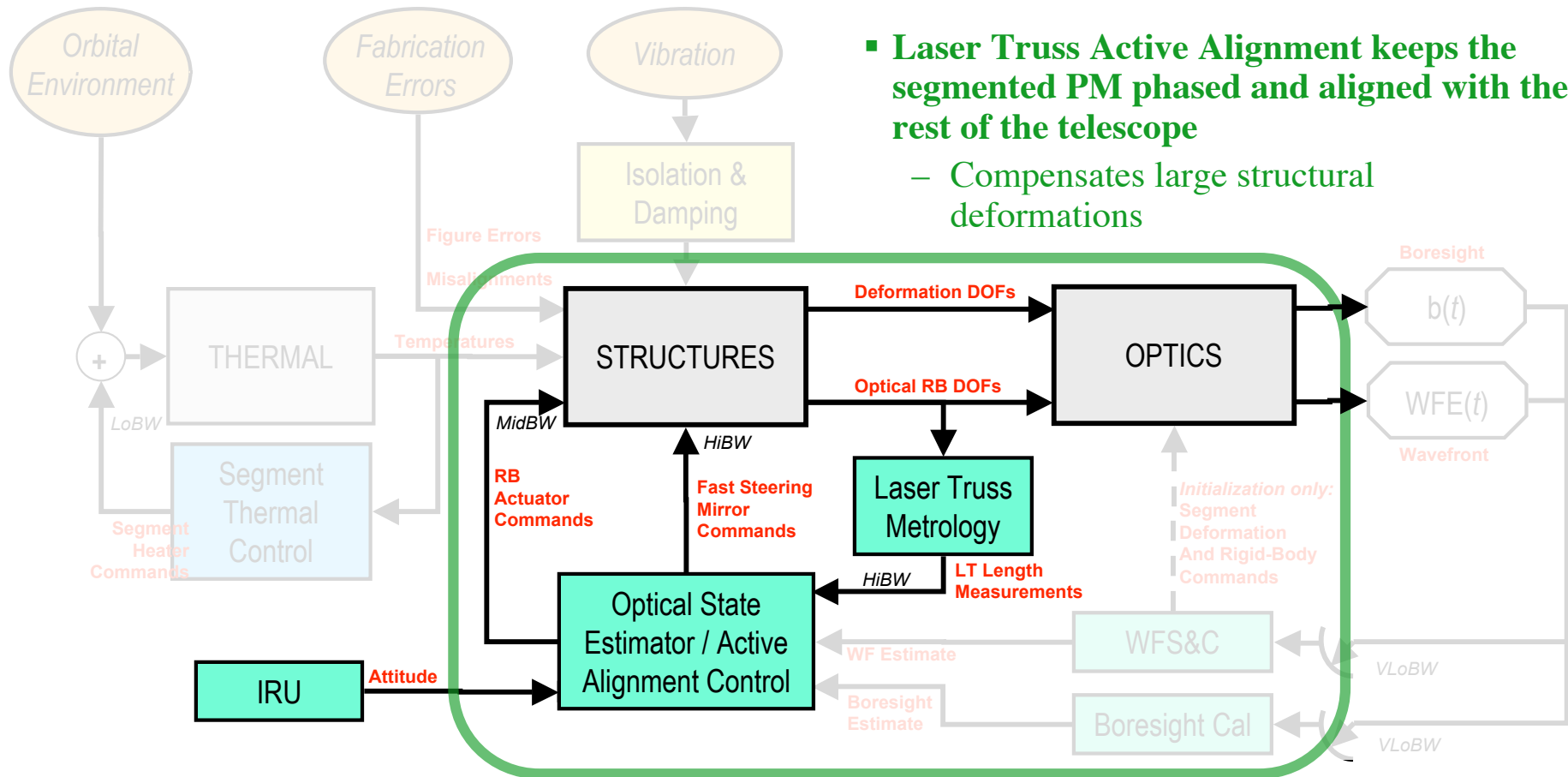


## ■ Segment figure is thermally stabilized

- Passive Athermalization: keeps WFE/°C very low
- Local Segment Thermal Control: PM segment temperatures are kept constant using heaters integrated with segment structure

# Laser Truss Keeps All Optics Aligned

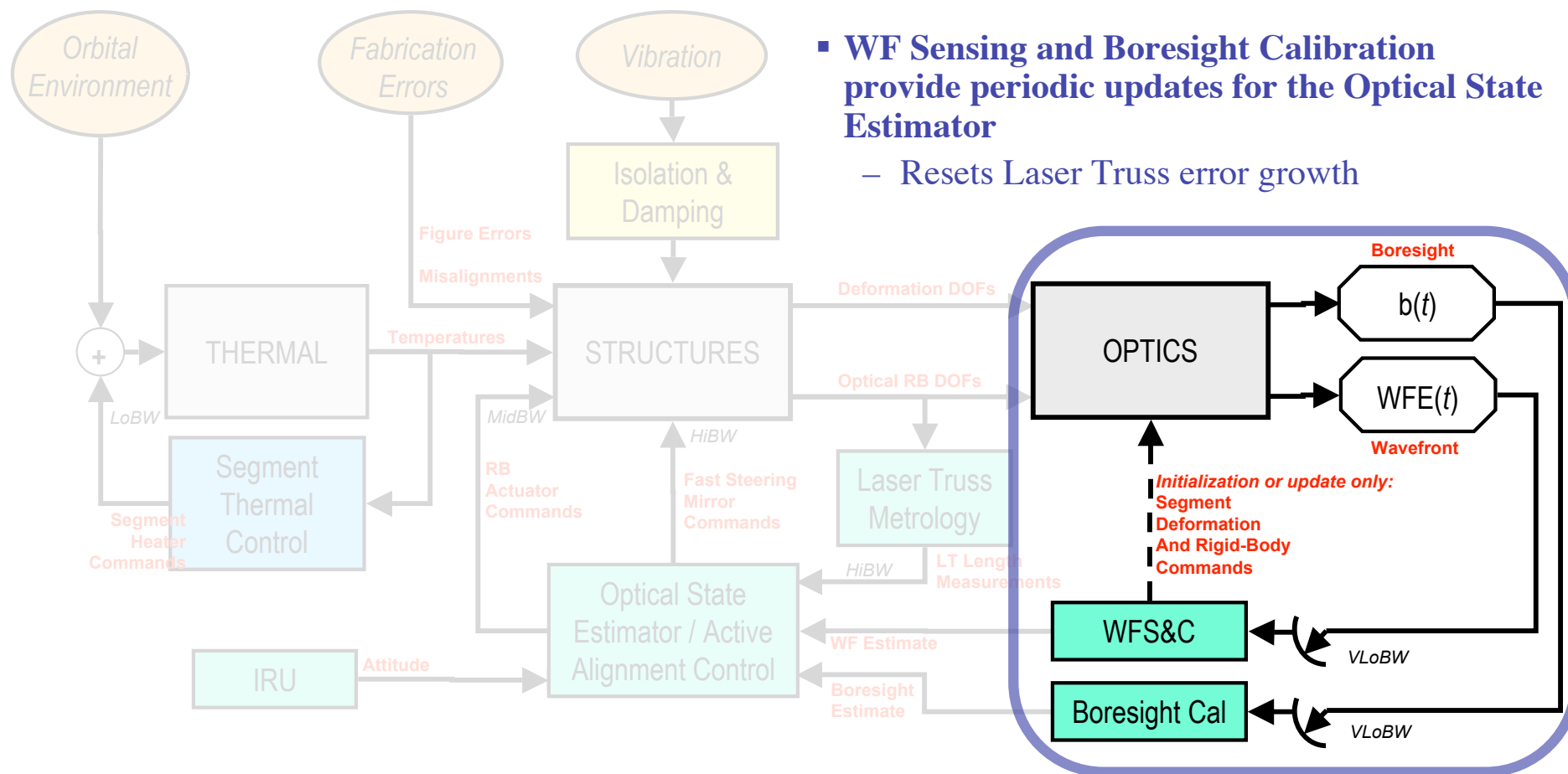
- Laser Truss Active Alignment keeps the segmented PM phased and aligned with the rest of the telescope**
  - Compensates large structural deformations



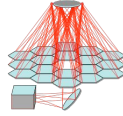
- Laser Truss measurements at high BW are processed in a Kalman Filter to estimate the perturbation state of all the optics**
- Estimated state is fed back to control WFE at low BW and boresight at high BW**

# WFS&C Updates

- **WF Sensing and Boresight Calibration provide periodic updates for the Optical State Estimator**
  - Resets Laser Truss error growth



- Laser Truss measurements at 100 Hz are processed in a Kalman Filter to estimate the perturbation state of all the optics
- Estimated state is fed back to control WFE ( $< 1$  Hz) and boresight ( $< 10$  Hz)



# Laser Truss Pros and Cons

## ■ Pros

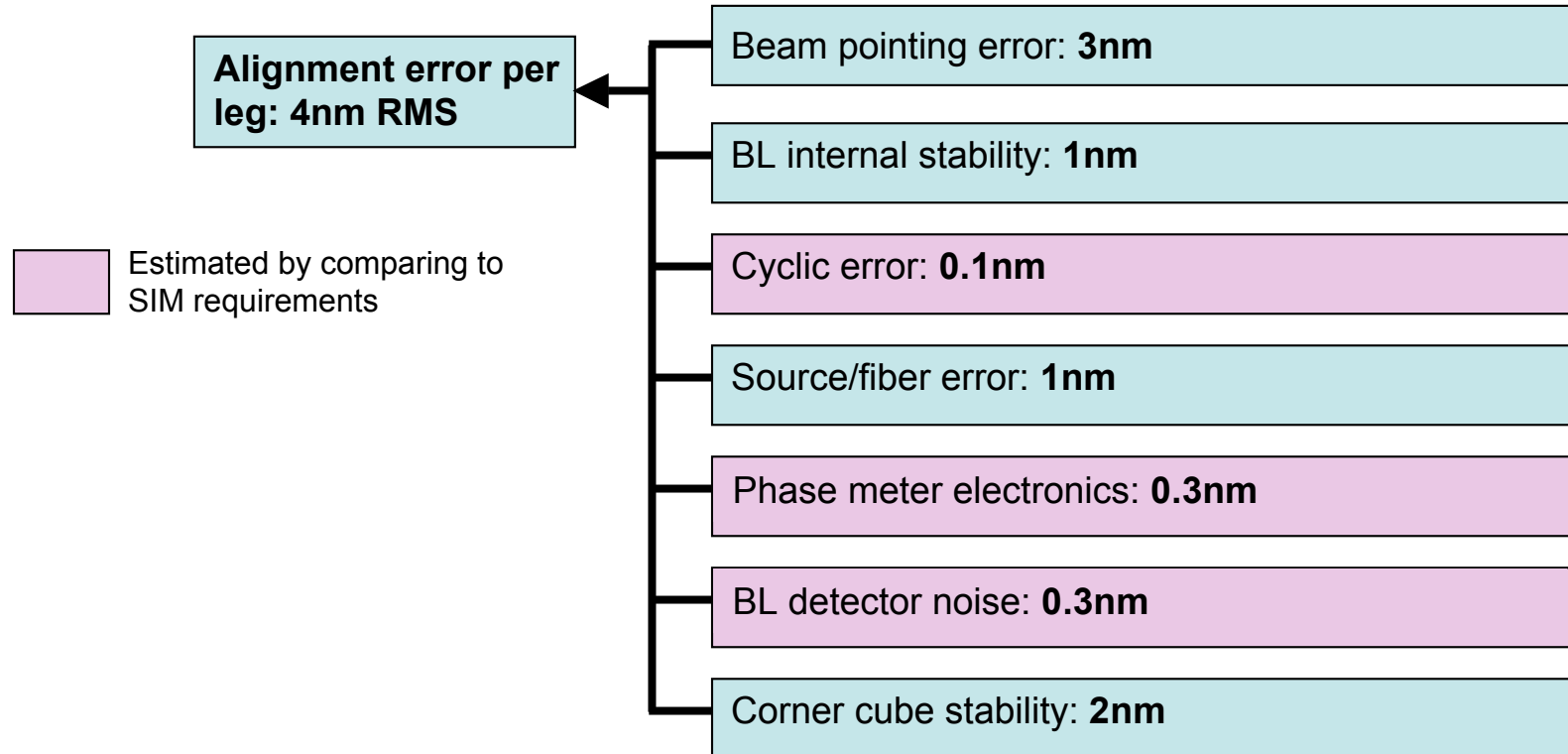
- High accuracy –  $< 1$  nm per LDG when  $\Delta$  angle is small
- Observes all important RB states – including Primary and Secondary Mirrors, and Optical Bench
- Low drift – with 1 laser feeding all LDGs, require WFS update once per day
- Light weight beam launchers
- No on-segment power dissipation
- Does not require segments to be close together
- Does not require any particular gap geometry
- Works with missing segments (no degradation for the segments that remain)
- Useful for I&T
- Degrades gracefully if individual LDGs go out

## ■ Cons

- Requires 12 fibers into each segment for 6 DOF

# Notional Metrology Error Budget

- Notional LDG error budget, based on extrapolated SIM and R&TD data



- This level of performance is much worse than was *demonstrated* by SIM
- However...
  - Much smaller, lighter-weight components will be needed
  - Long-term laser frequency stability will be required



## Conclusion

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- **Our baseline utilizes developing and realized active optics technologies to provide a plausible development path to diffraction limited performance at 500 nm wavelength for ATLAS-T16**
- **Planet Imaging will require further active optics technology development**
  - Large lightweight segments
  - Smaller, lighter, higher performance LDGs
  - On-board closed-loop extreme WF sensing and control
  - Broad-band coronagraphy