

# **Novel Technology for Ultra-Sensitive Cosmology Instruments**

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**University of Oxford**

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# Technology for Ultra-Sensitive Cosmology Instruments

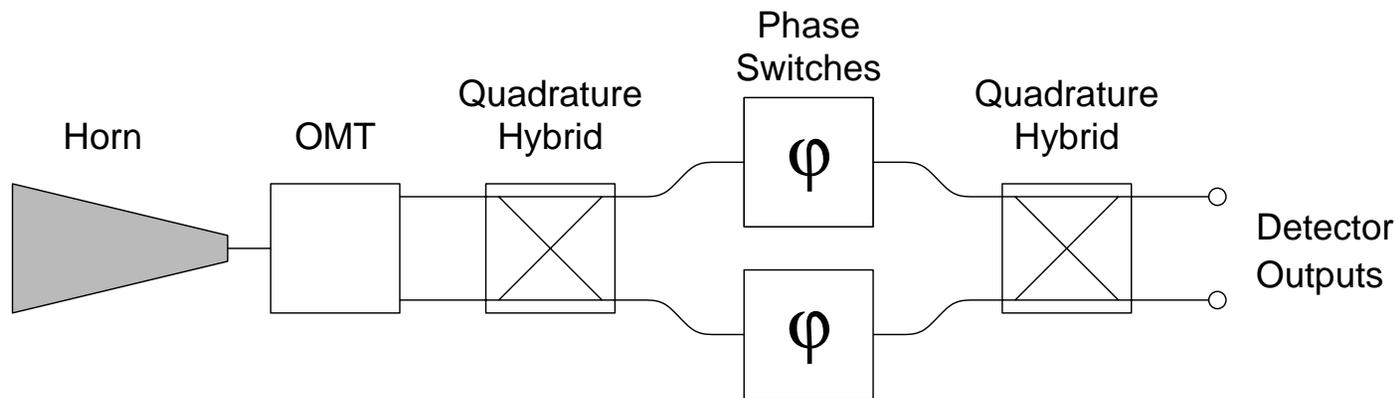


- CMB B-mode science requirements.
- Instruments Design
- Telescope
- **Feed arrays**
- **Phase modulation**
- **Detectors**

## Why Phase Modulate?



- Reduce 1/f noise
- Measure Stokes parameters without moving correlation receiver components

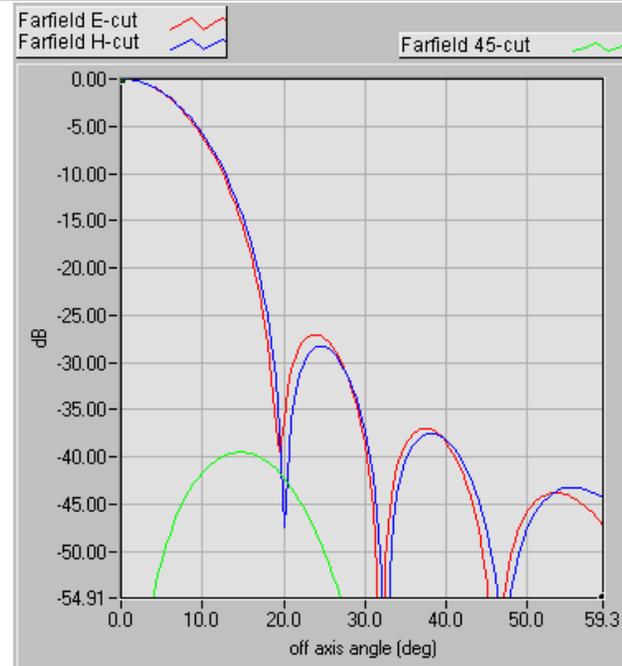
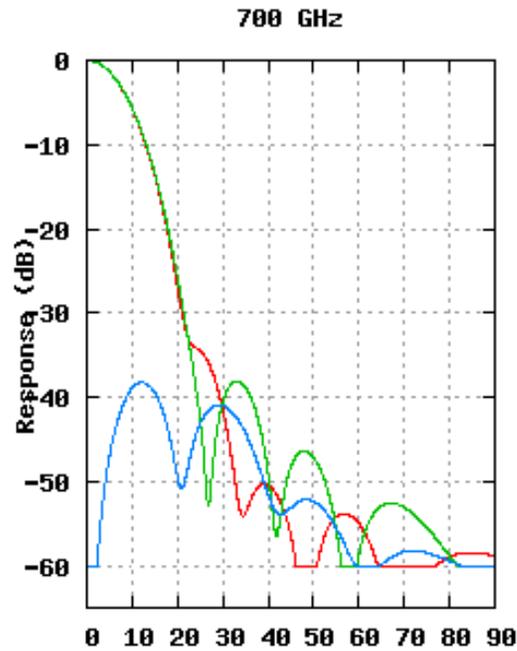


$$D1 = I - Q \cos \psi - U \sin \psi$$

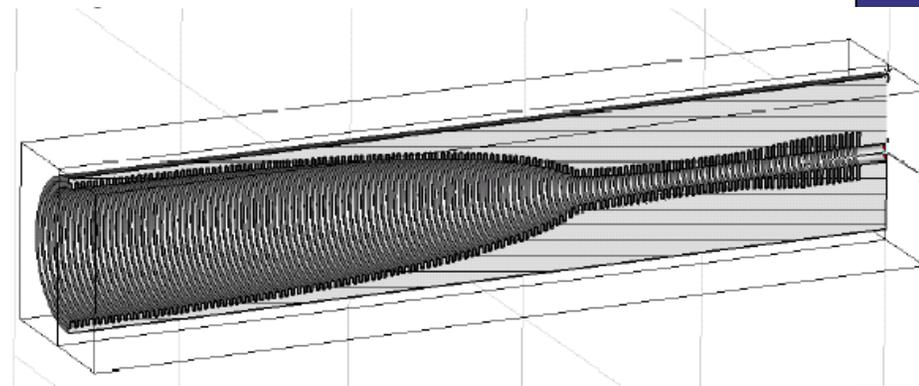
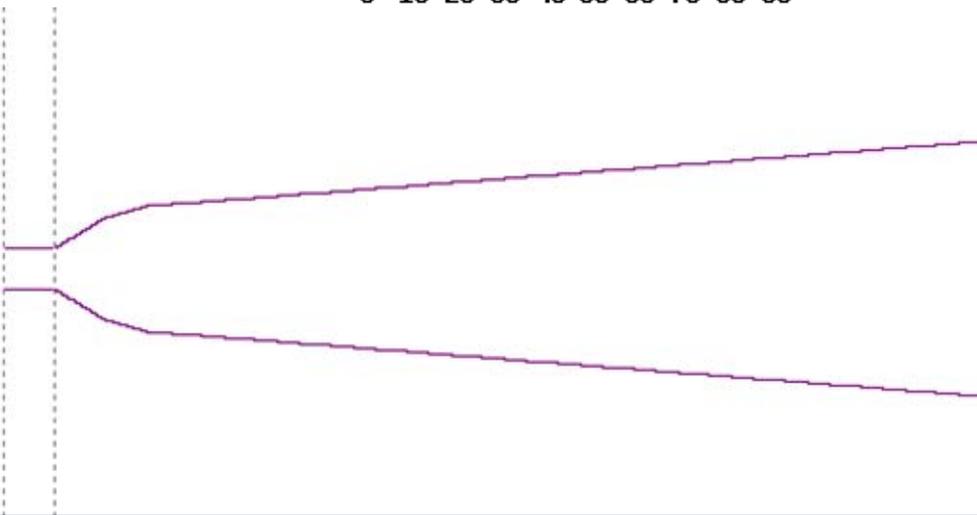
$$D2 = I + Q \cos \psi + U \sin \psi$$

# Multi-flare (smooth-walled)

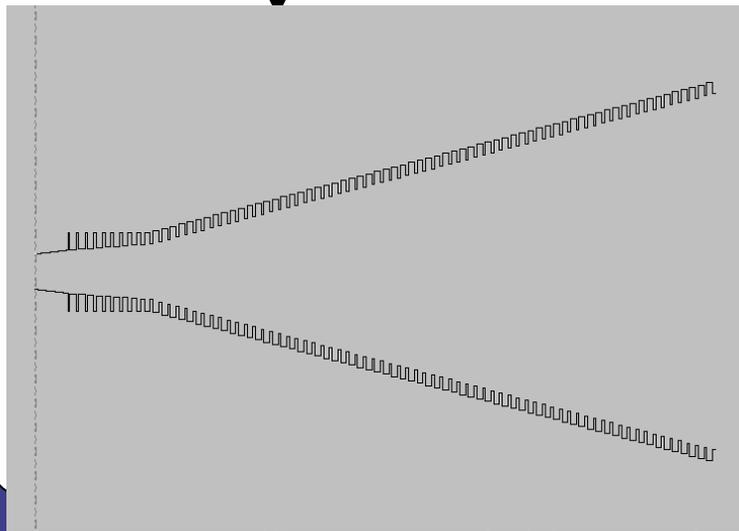
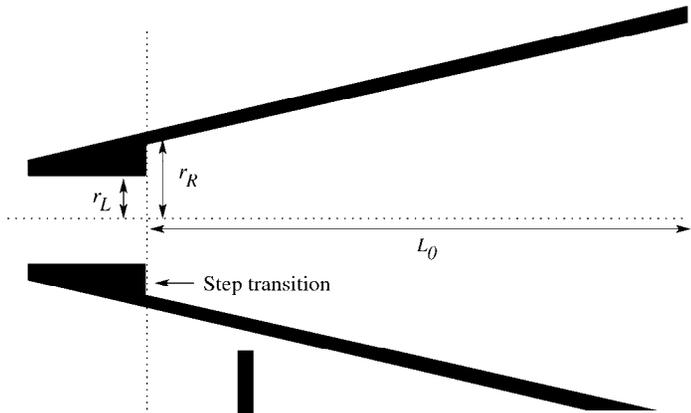
Three  
flare-  
steps  
horn



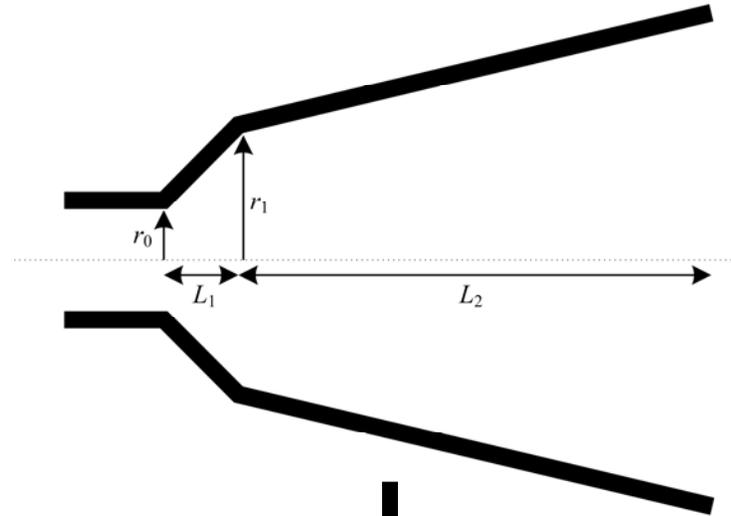
Profiled  
Corrugated  
horn



# Generalize to a wideband horn



Experimental Cosmology Group



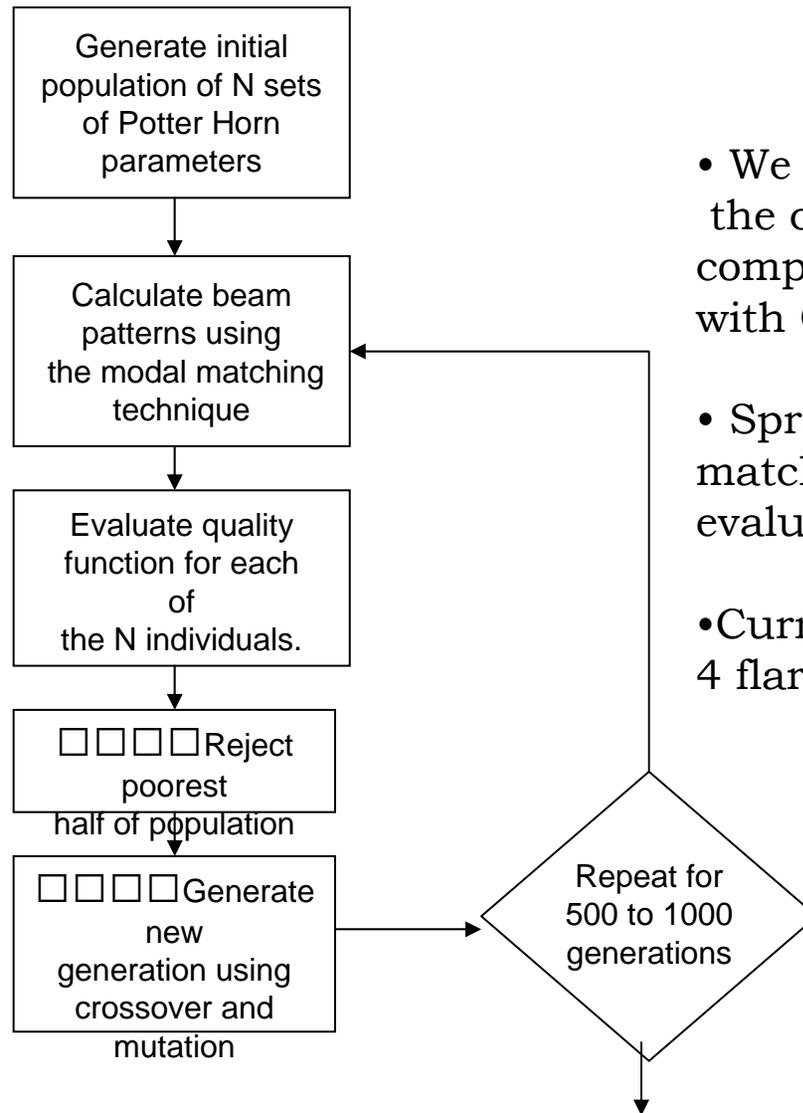
Oxford Astrophysics

## *Hornsynth Software Package*



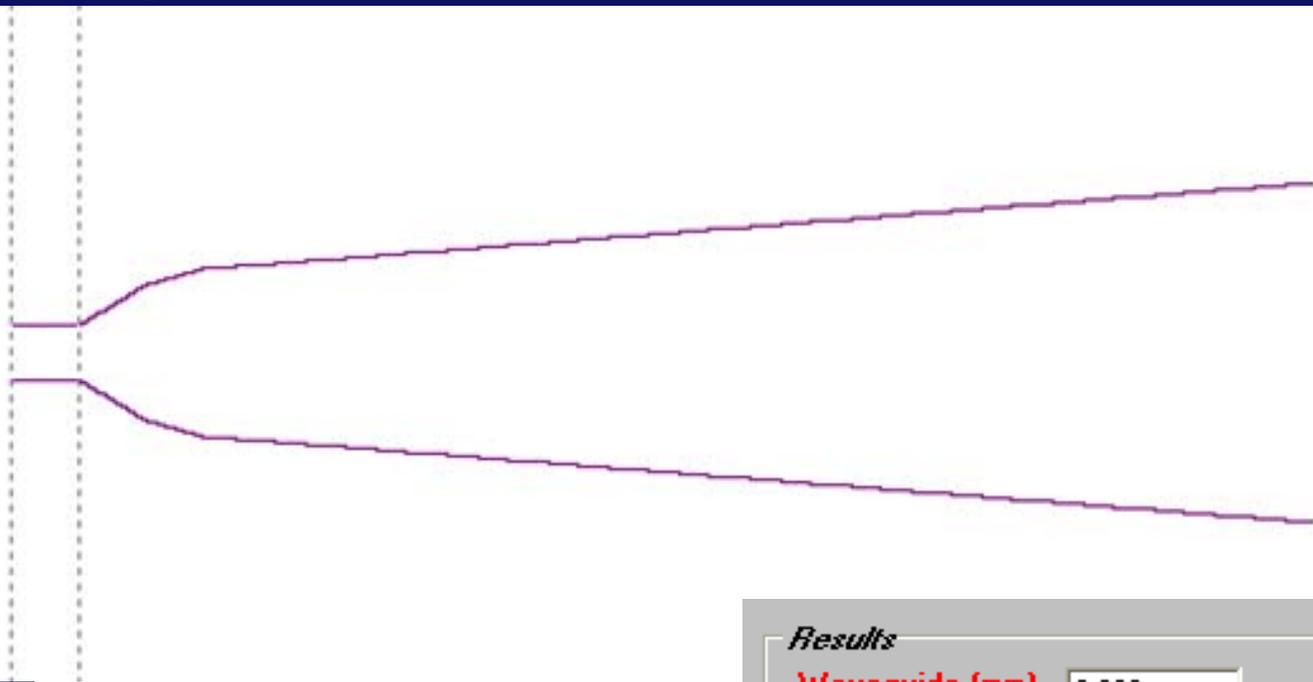
- Written by P. Kittara , A. Jiralucksanawong (Mahidol University, Thailand) in collaboration with Ghassan Yassin (Oxford Physics)
- It consists of two software packages: (1) modal matching software (2) Optimization software
- The minimization package is a Genetic Algorithm routine and a Simplex routine
- The software searches for the global minima according to a “fitness” criteria. In our case it is the circularity and cross-polarization level.

# Design using a Genetic Algorithm (GA)



- We have successfully parallelized the code to run over the UK GRID computing system, in collaboration with Oxford eScience.
- Spread processor intensive modal matching and quality function evaluation over multiple processors.
- Currently optimizing designs with 4 flare angles.

# Three angles horn design



**Hornsynth**  
output

*Results*

|                       |   |   |   |                                  |
|-----------------------|---|---|---|----------------------------------|
| <b>Waveguide (mm)</b> | <input type="text" value="0.200"/>      |   |   |                                  |
|                       | <b>Begin R</b>                          | <b>Length</b>                           | <b>End R</b>                            | <b>Section</b>                   |
| <b>Section 1 (mm)</b> | <input type="text" value="2.00000E-1"/> | <input type="text" value="4.85800E-1"/> | <input type="text" value="4.88400E-1"/> | <input type="text" value="49"/>  |
| <b>Section 2 (mm)</b> | <input type="text" value="4.88400E-1"/> | <input type="text" value="3.98310E-1"/> | <input type="text" value="5.95277E-1"/> | <input type="text" value="30"/>  |
| <b>Section 3 (mm)</b> | <input type="text" value="5.95277E-1"/> | <input type="text" value="7.88560E+0"/> | <input type="text" value="1.200"/>      | <input type="text" value="110"/> |
| <b>Error Fuction</b>  | <input type="text" value="3.99830E-5"/> | <input type="text" value="3.99830E-5"/> |   |                                  |

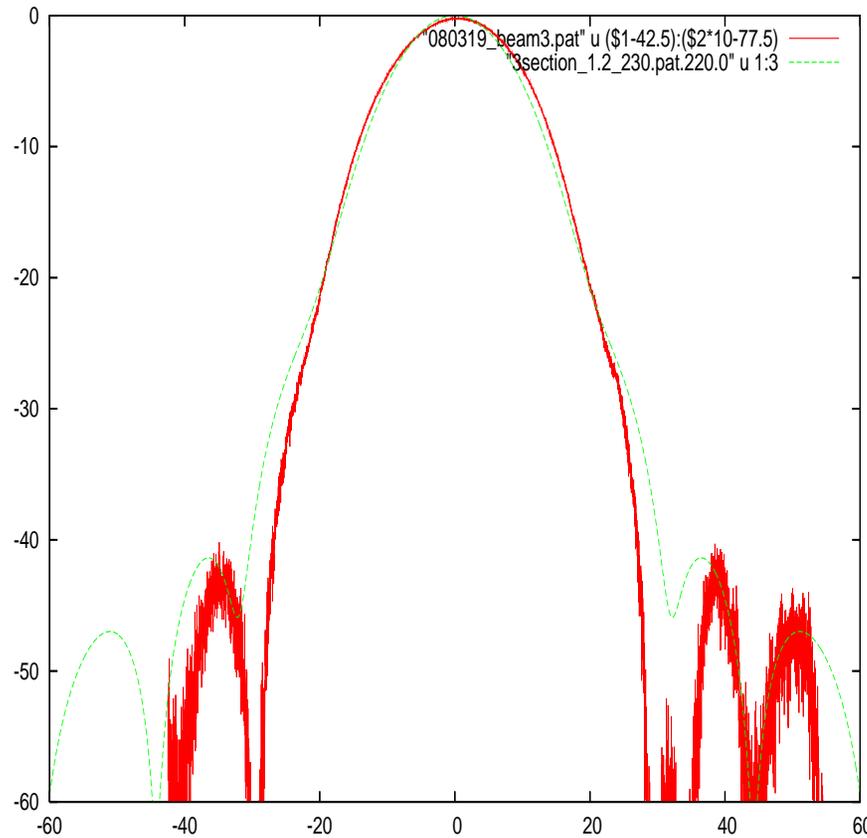
# Horn dimensions at 230 GHz



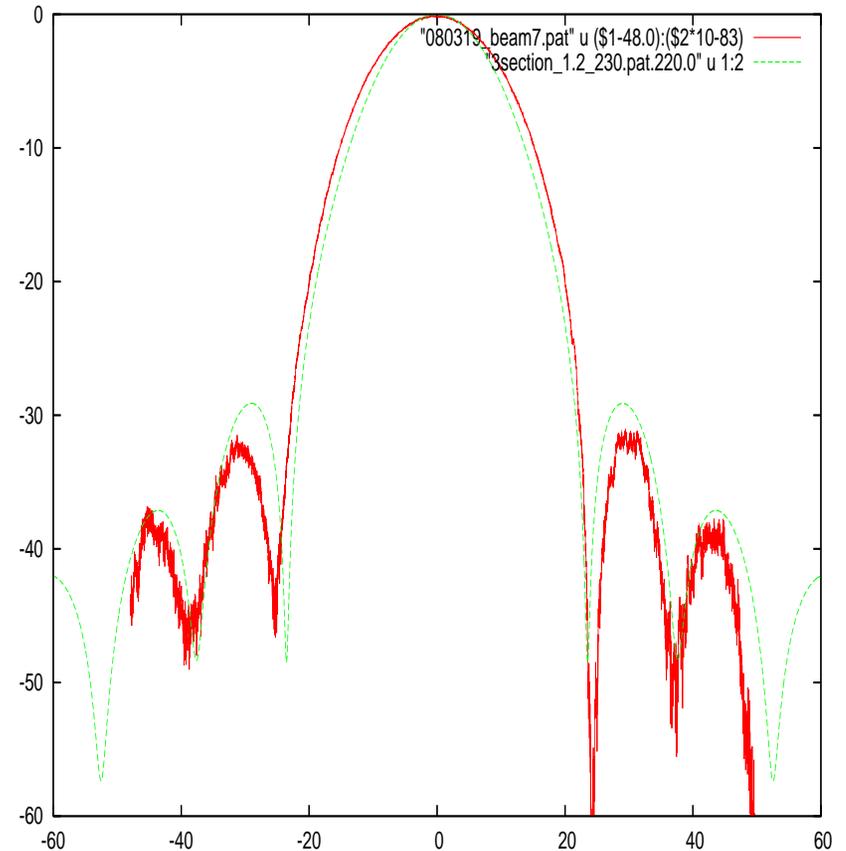
|  |           |
|--|-----------|
| Initial waveguide radius,                      | 1.24 (mm) |
| Length of the 1 <sup>st</sup> conical section, | 1.479     |
| Radius of the 1st conical section,             | 1.486     |
| Length of the 2nd conical section,             | 1.212     |
| Radius of the 2st conical section,             | 1.812     |
| Length of the 3rd conical section,             | 2.4       |
| Aperture                                       | 3.652     |
|  |           |

**Green: Theory**

**Red: Measured**

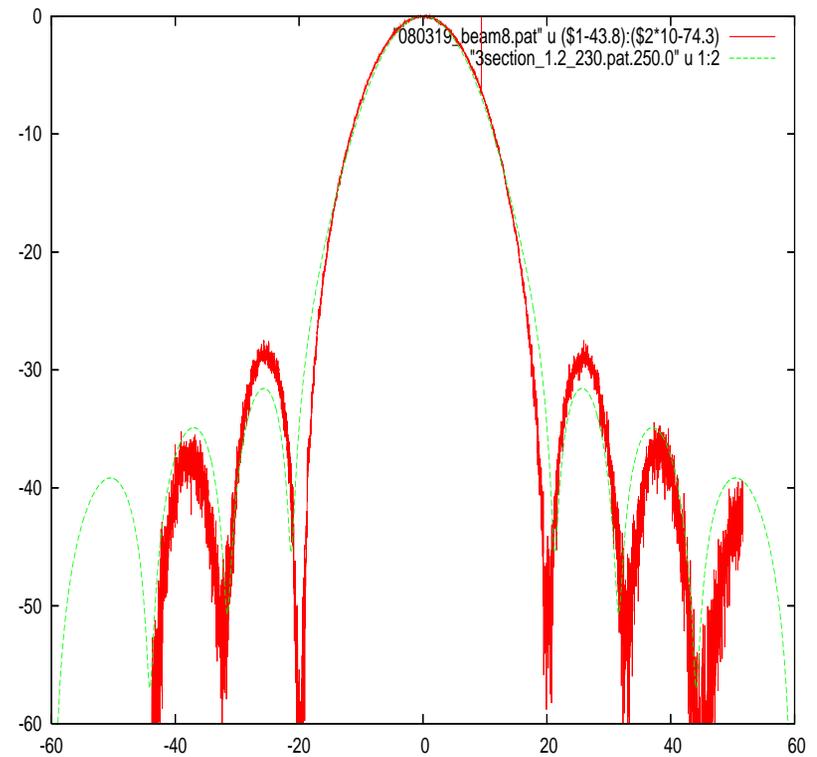
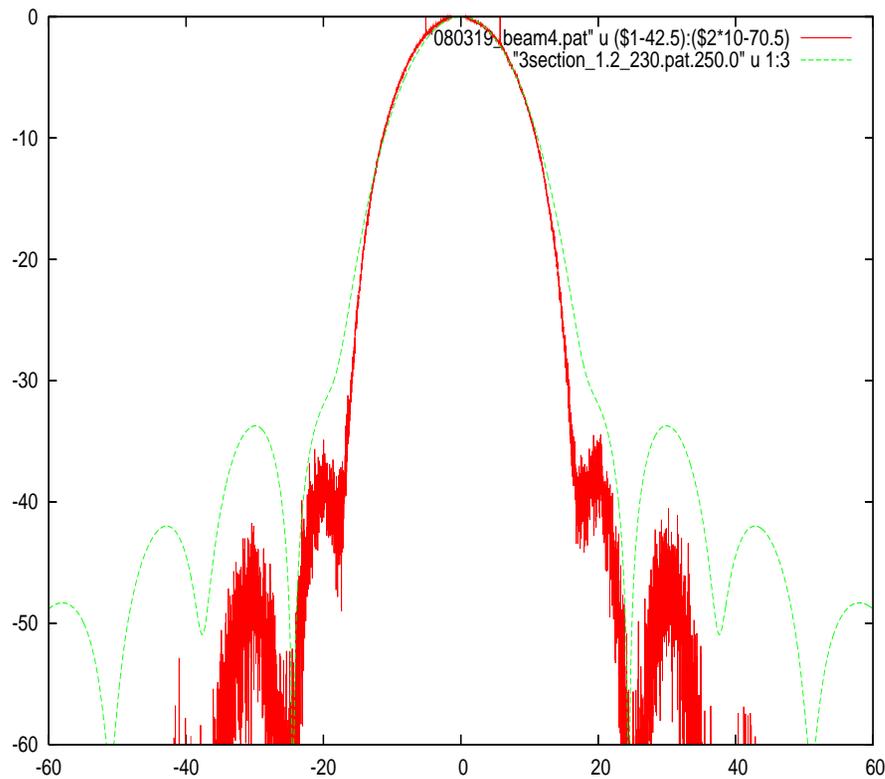


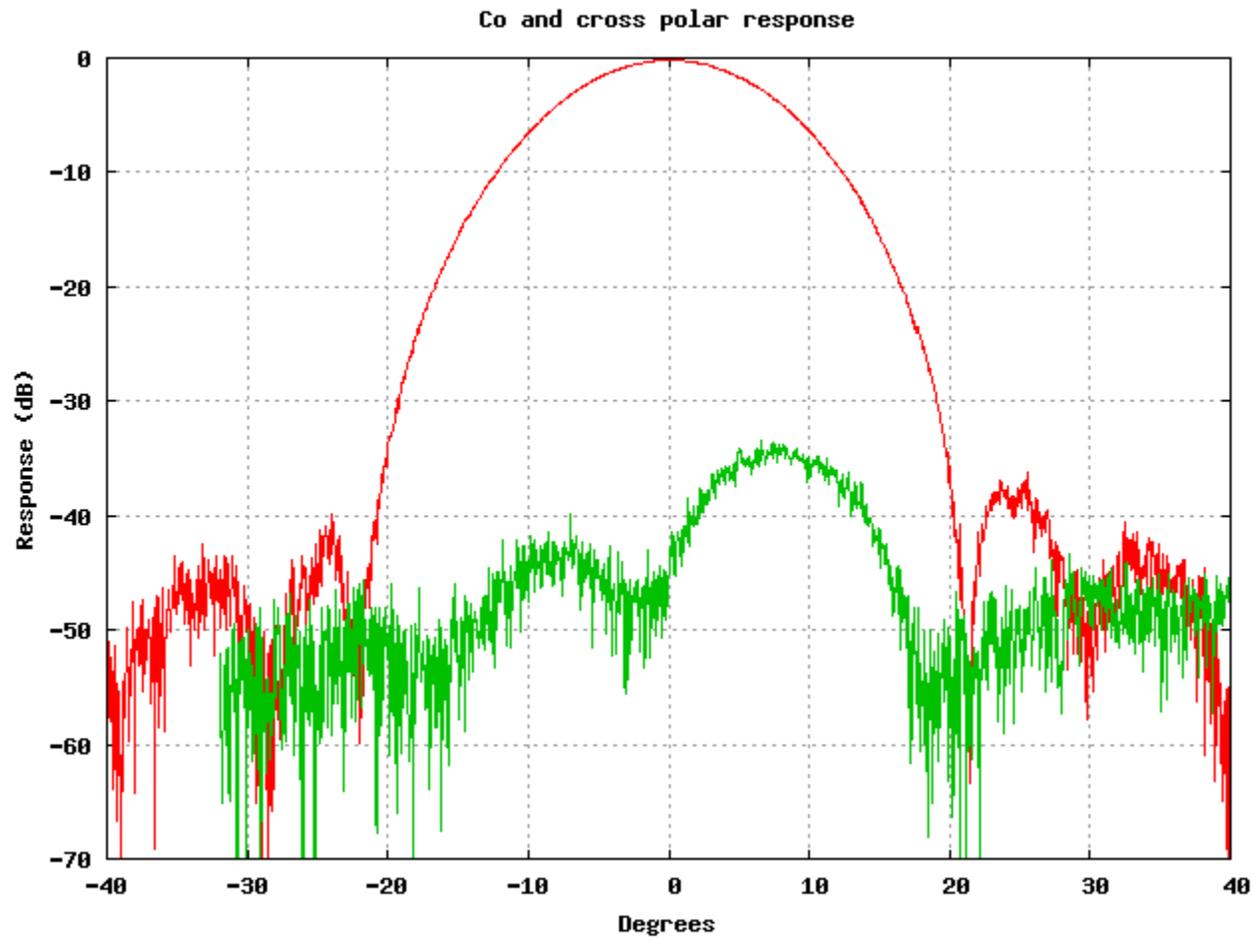
**H-plane**



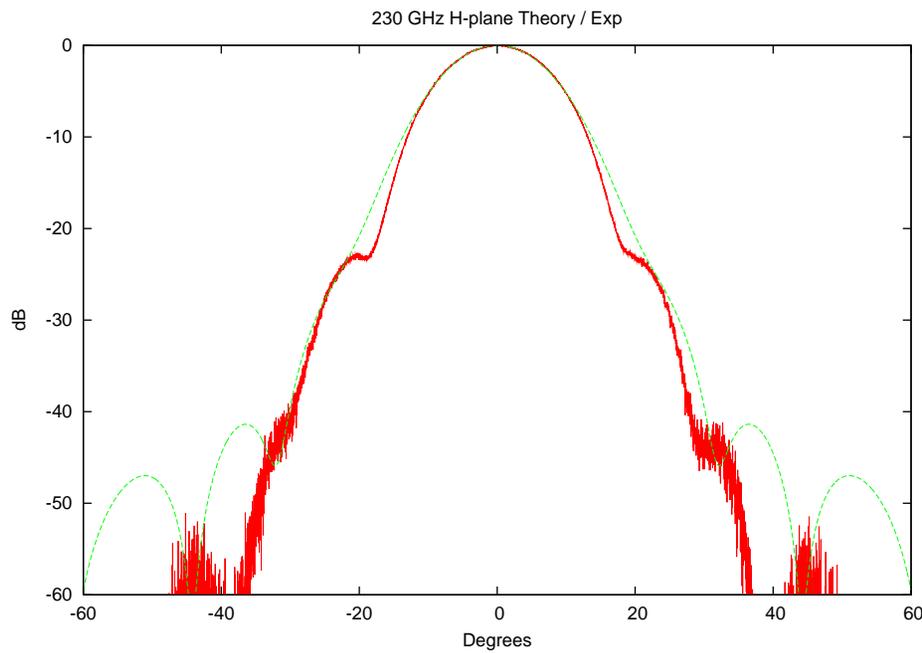
**E-plane**

## Pattern at 250 GHz



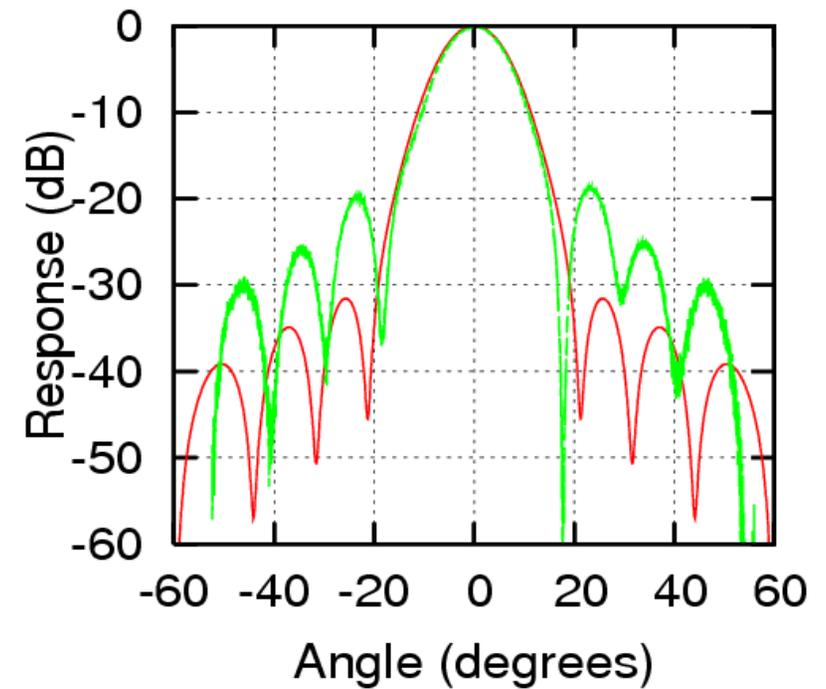


# Drilling Technology



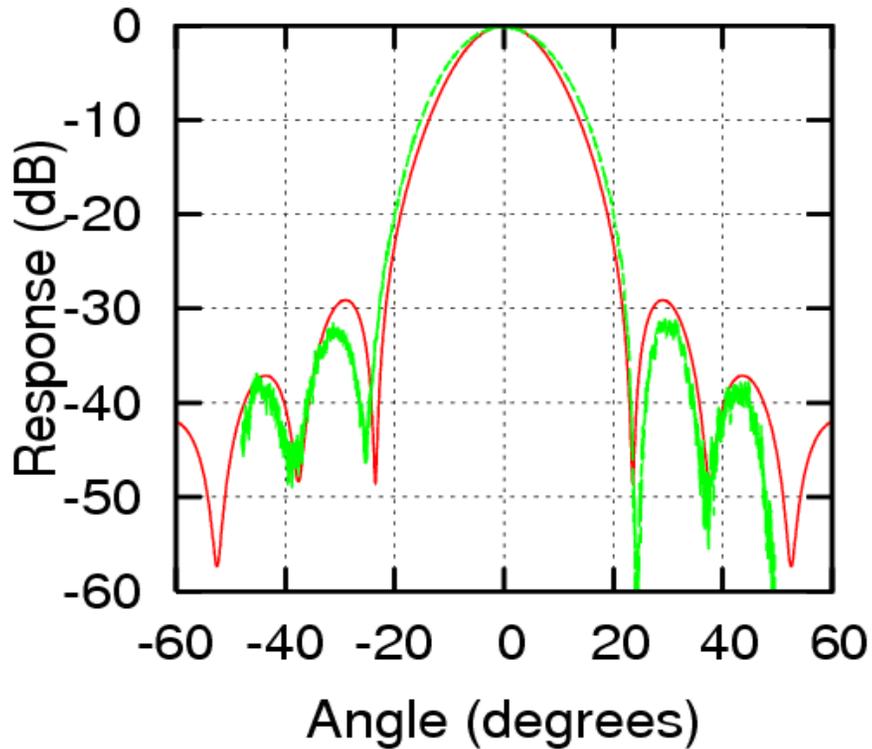
Experimental Cosmology Group

## 250 GHz E-plane Theory and Experiment

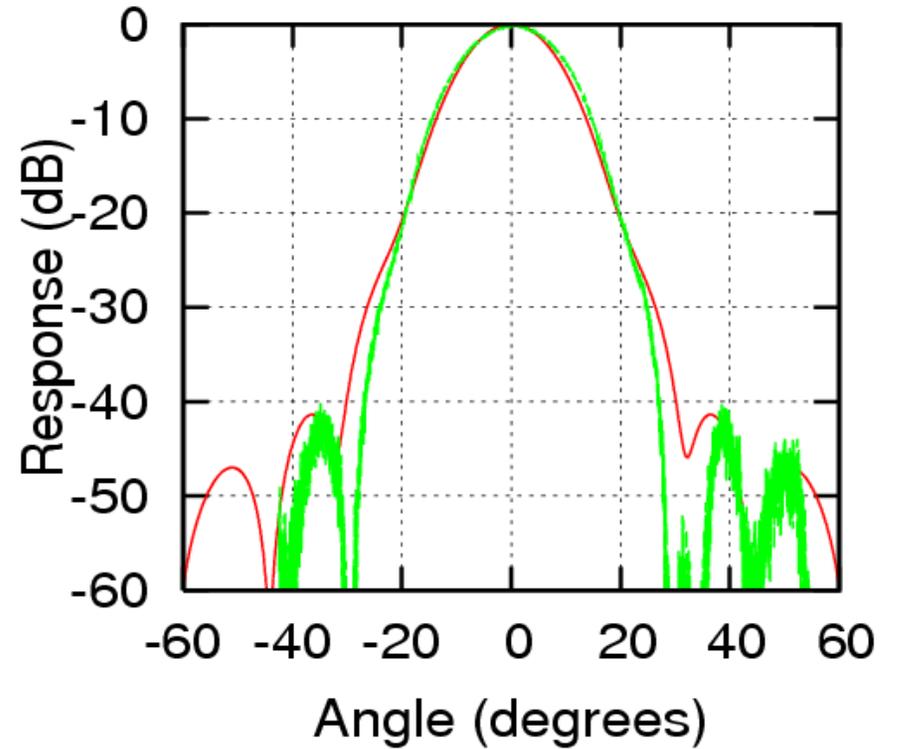


Oxford Astrophysics

220 GHz E-plane  
Theory and Experiment

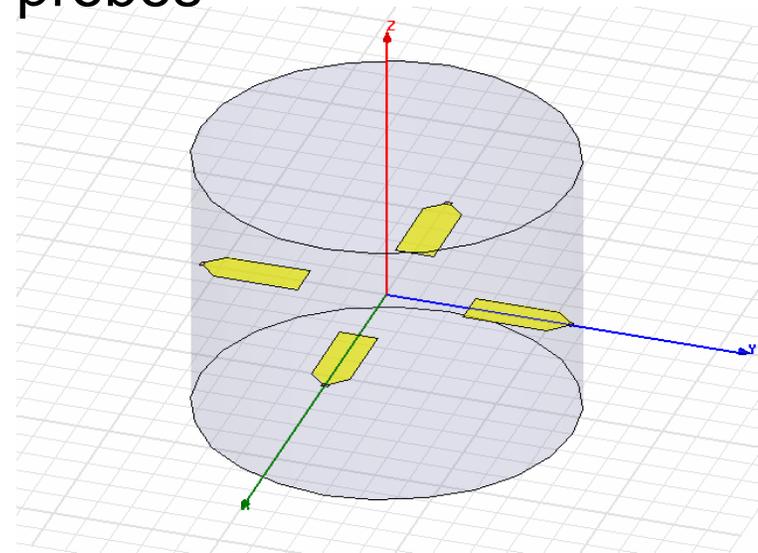
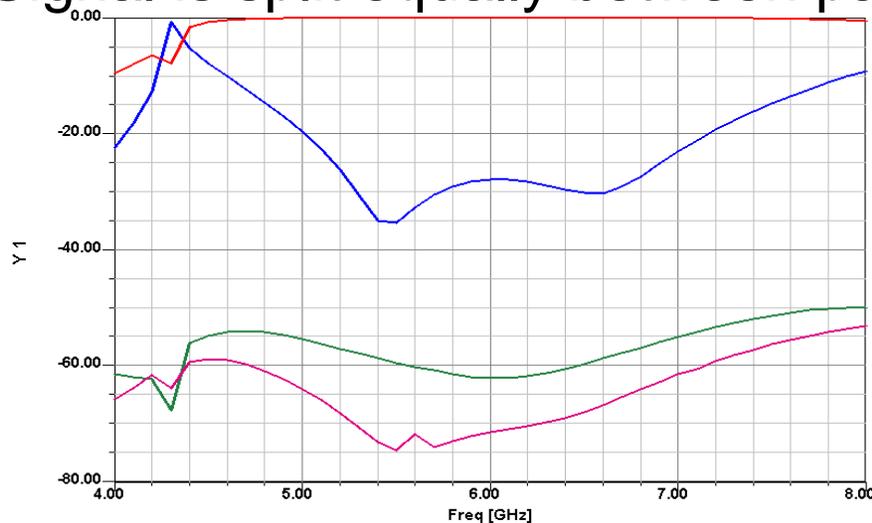


220 GHz H-plane  
Theory and Experiment



# Four probe OMT

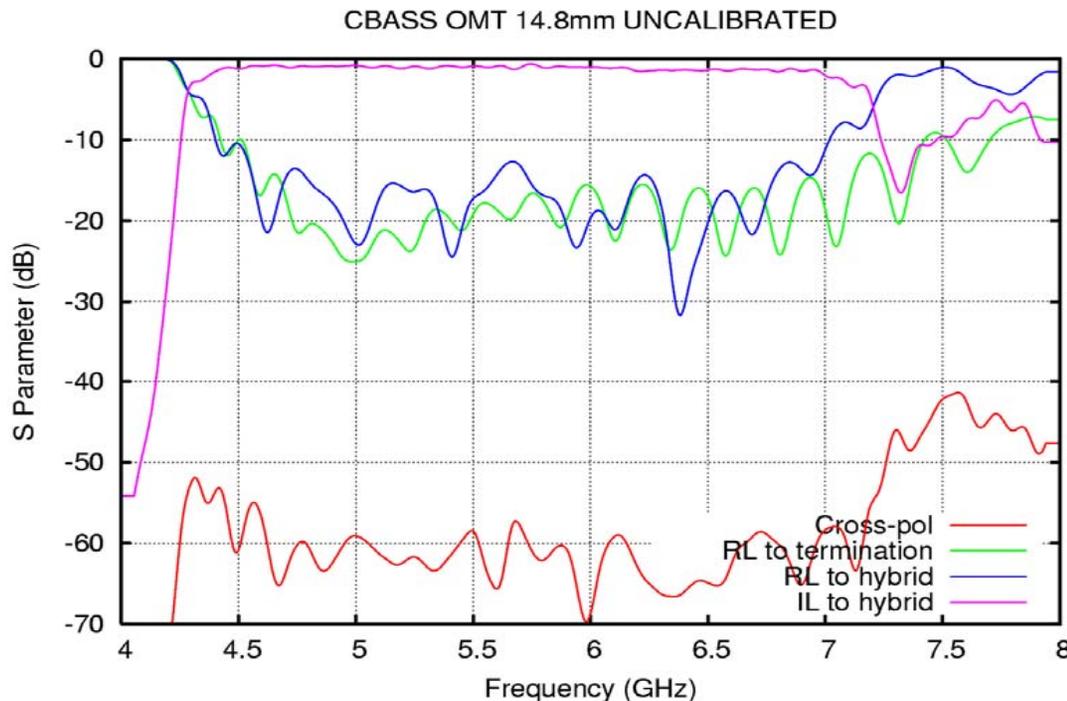
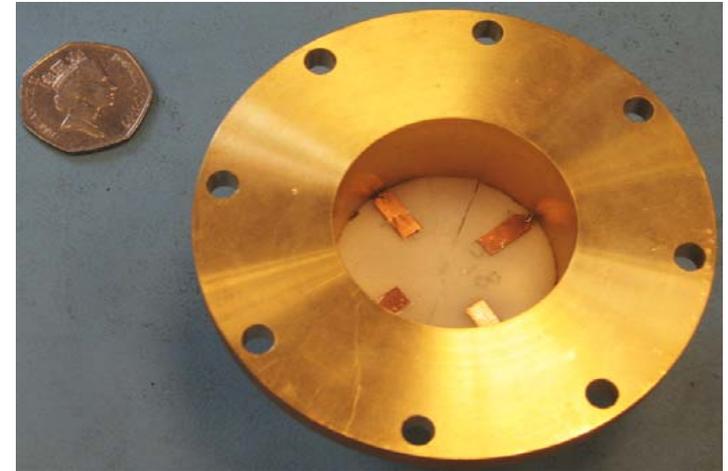
- Combine orthomode transducer and waveguide to transmission line coupling in single on-chip structure
- 4 rectangular probes in circular waveguide
- Probes sit in front of waveguide backshort
- Each pair of probes only respond to one polarization mode
- Signal is split equally between pair of probes



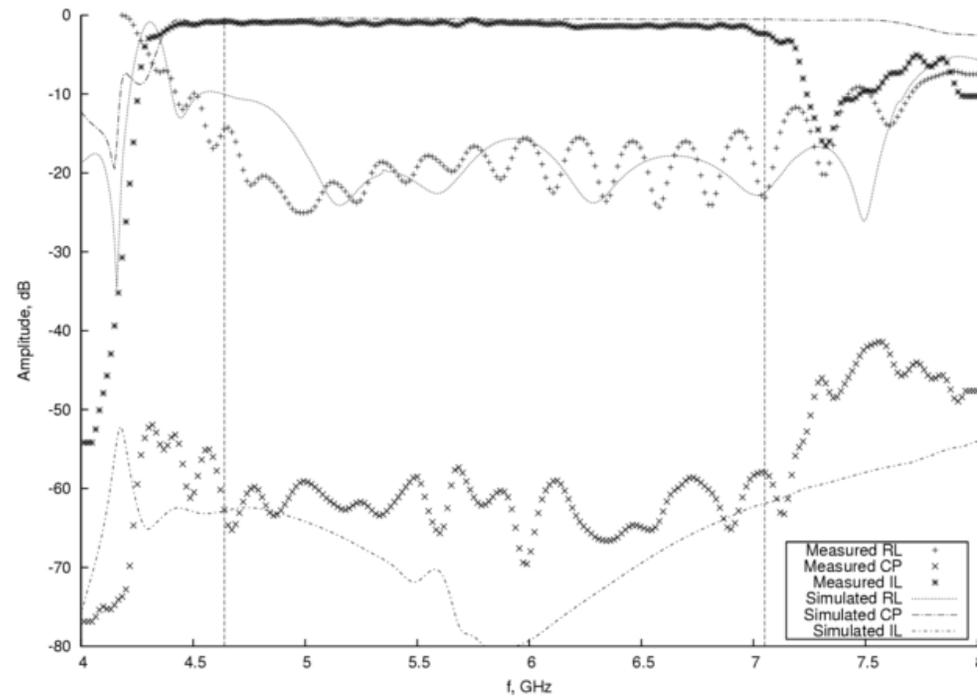
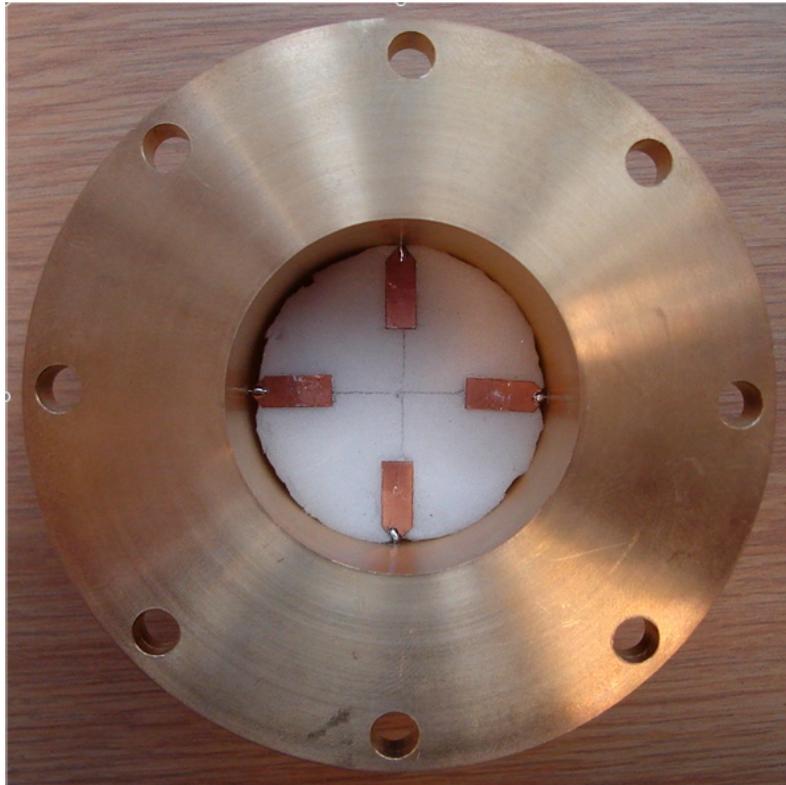
- Recombine signals in  $180^\circ$  hybrid, or send to separate detectors
- Hybrid improves cross-polar rejection - usually by  $> 20$  dB
- Design is optimised in HFSS to give best return loss and cross-polar performance over desired band

# Four probe OMTs in action

- 4 probe OMTs have been developed for C-BASS, a 5 GHz polarimeter, and the 150 and 225 GHz channels of Clover
- Now working on OMT for 350 GHz CEB



# CBASS OMT at 5 GHz

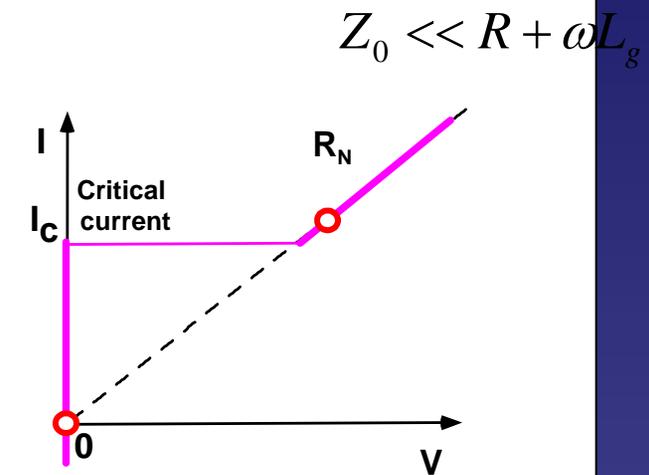
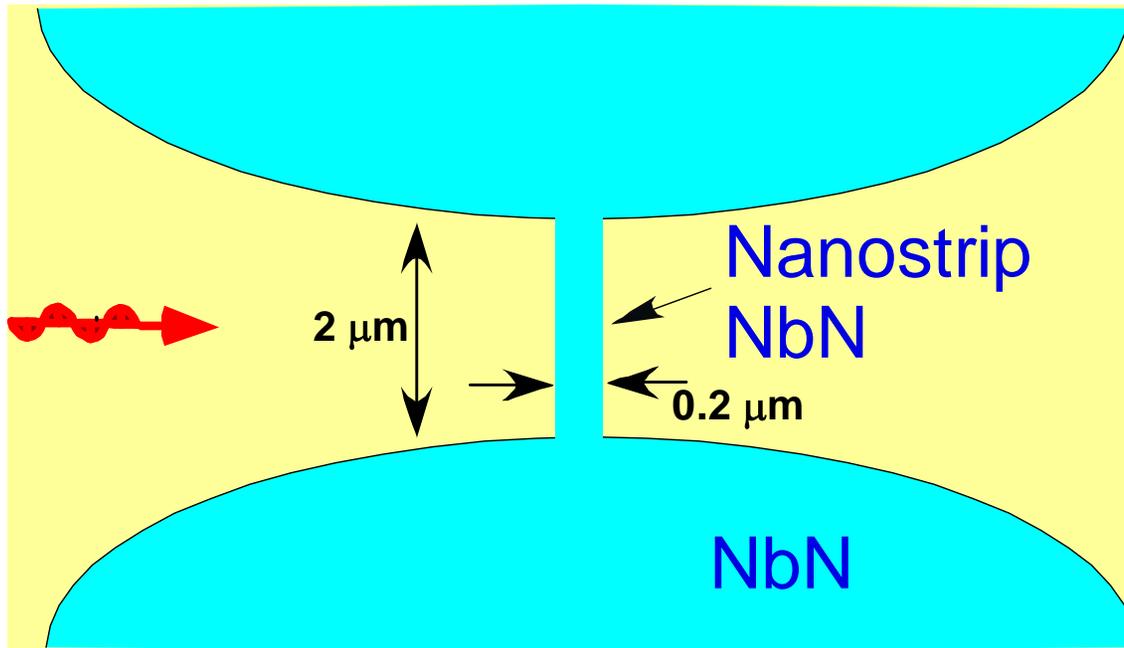


Grimes *et al Electron Lett.*, 43, 1146, 2007

- Mechanical rotation: difficult and expensive to realise and mass produce in cryogenic environment and expensive
- Faraday Rotor Ferrite Rods: difficult to mass-produce and lossy.
- Rotating Wave-plate: Obstructs the array can suffer from anisotropy.

- Collaboration between **Oxford** and **Chalmers**
- References:
  - Yassin, G., Kuzmin, L. S., Grimes, P., Tarasov, M., Otto, E. and Mauskopf, P. D. (2007) “An Integrated Superconducting Phase Switch for Cosmology Instruments” *Physica C: Applied Superconductivity and Application*, vol. 466 (issue 2) pp. 115-123
  - Kuzmin, L.S., Tarasov, M., Otto, E., Yassin, G., Grimes, P. K., and Mauskopf, P. D. (2007): “Superconductive sub-Terahertz nanoswitch,” *JETP Letters*, vol. 86 no. 4 pp. 275-277.

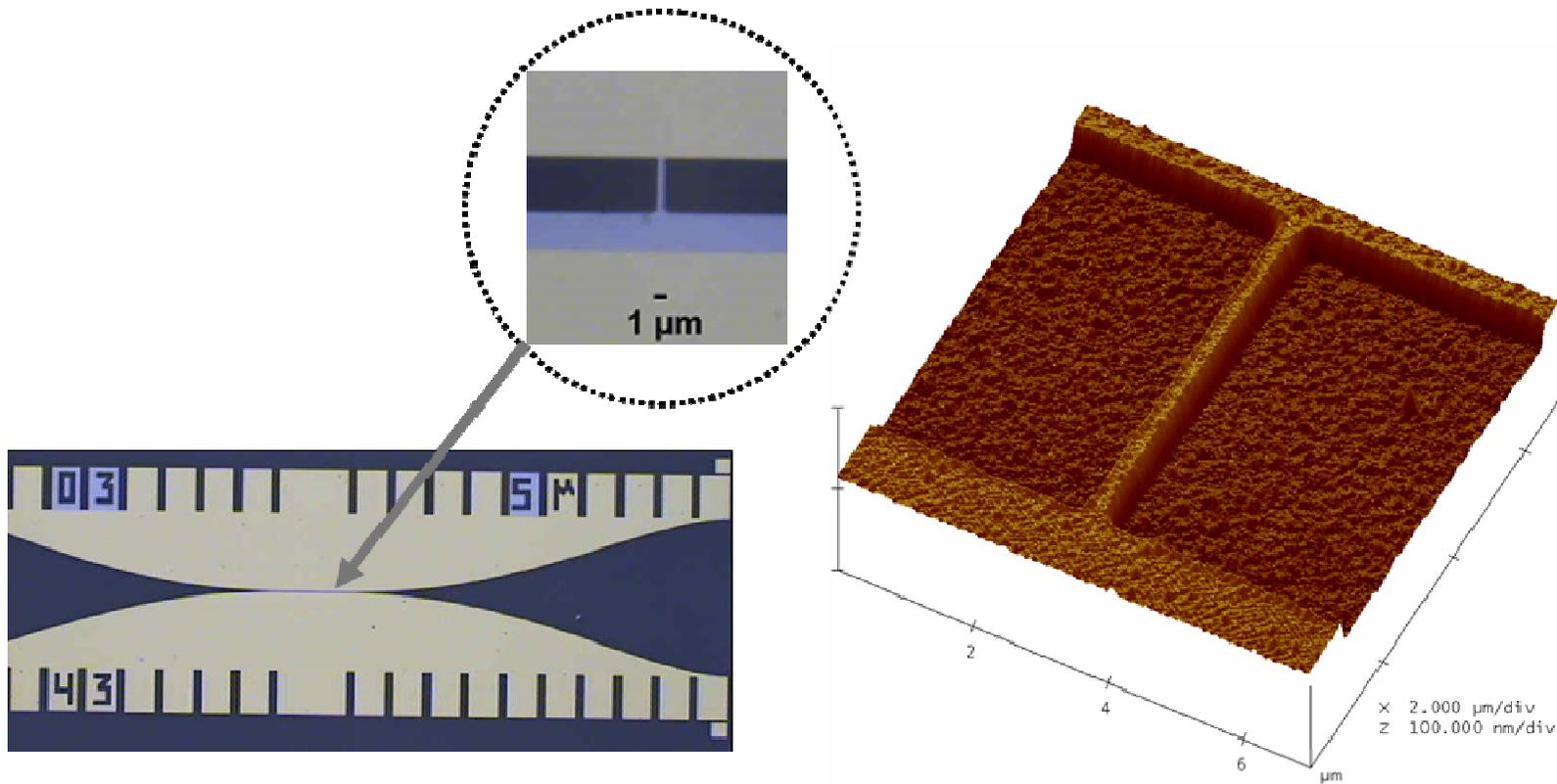
## NbN Nanostrip Switch

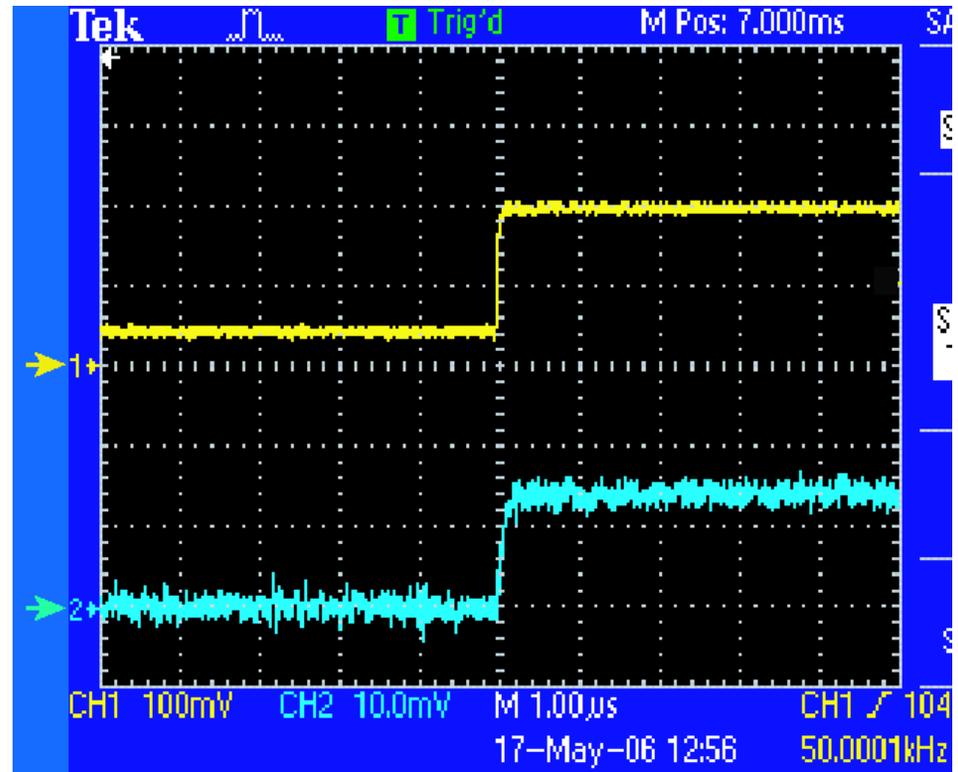
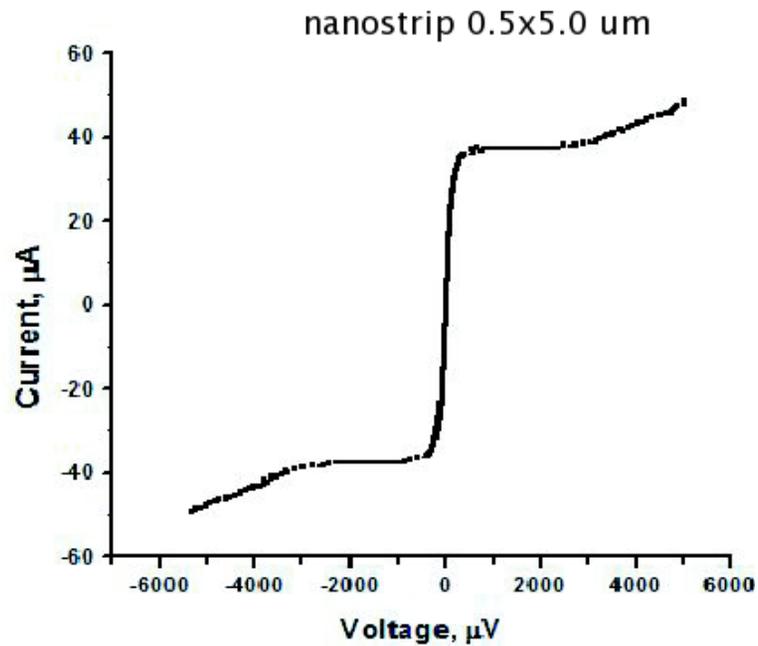


$$\omega L_c + \omega L_g \ll Z_0 \ll R$$

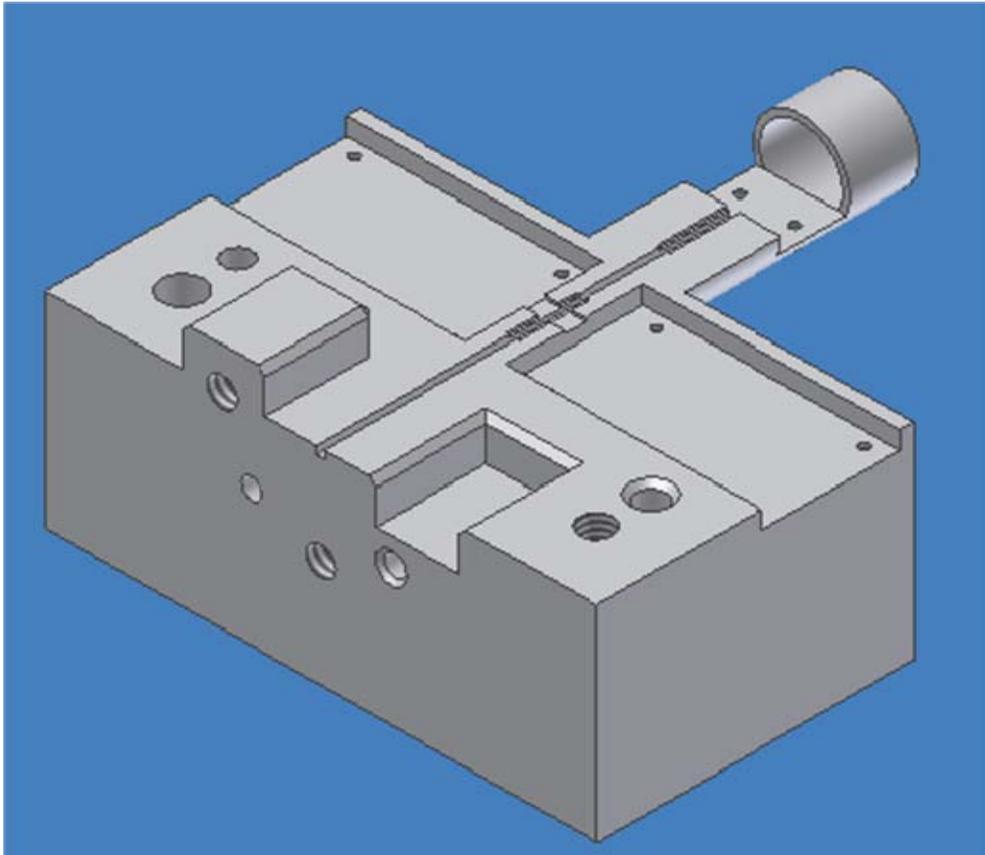
$$I_c = j_c * S, \quad L_c = \frac{\hbar}{2eI_c}, \quad R = \rho \frac{l}{S}$$

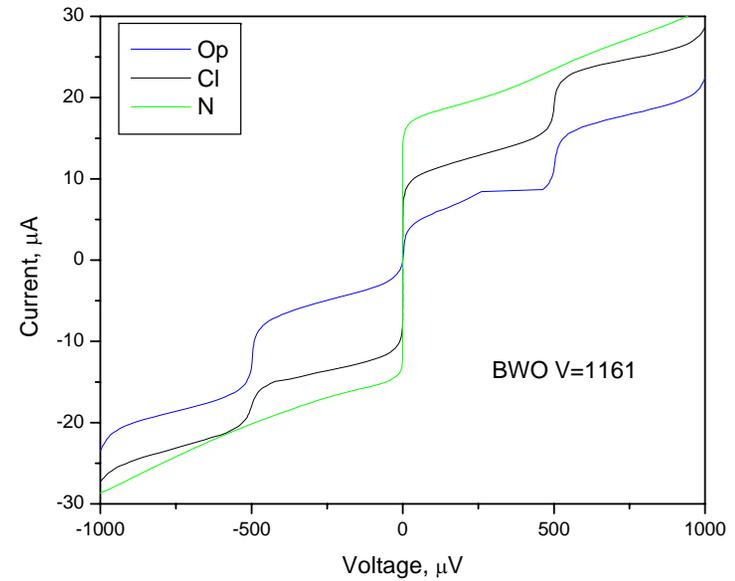
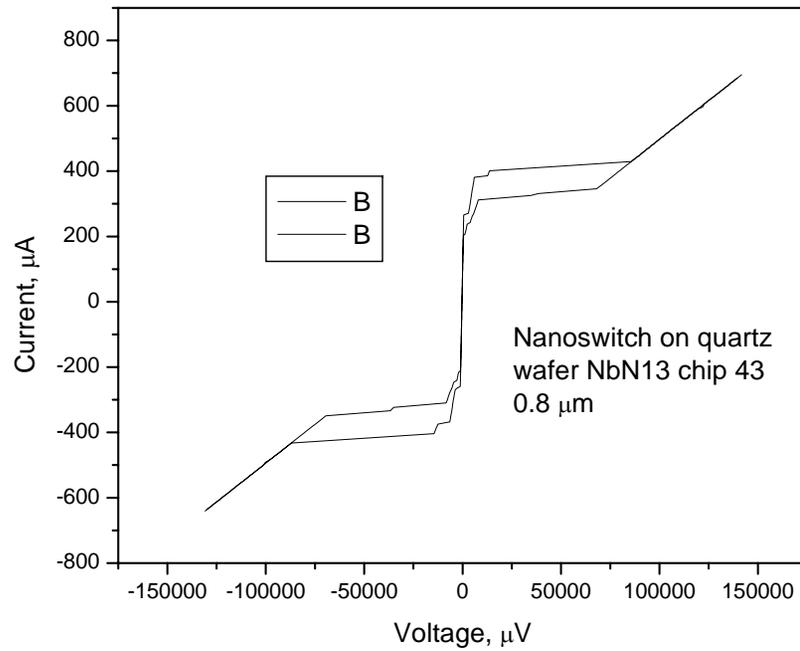
# Devices fabricated at Chalmers

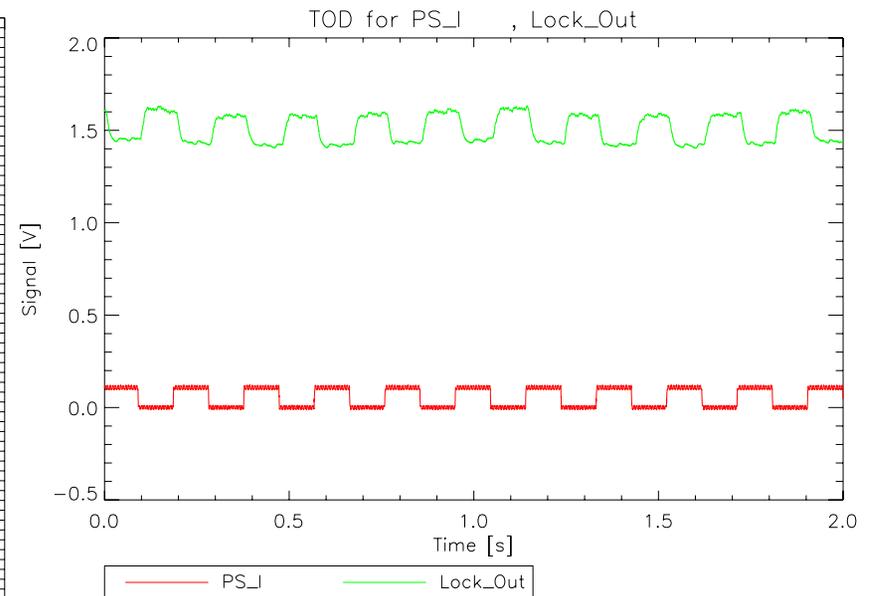
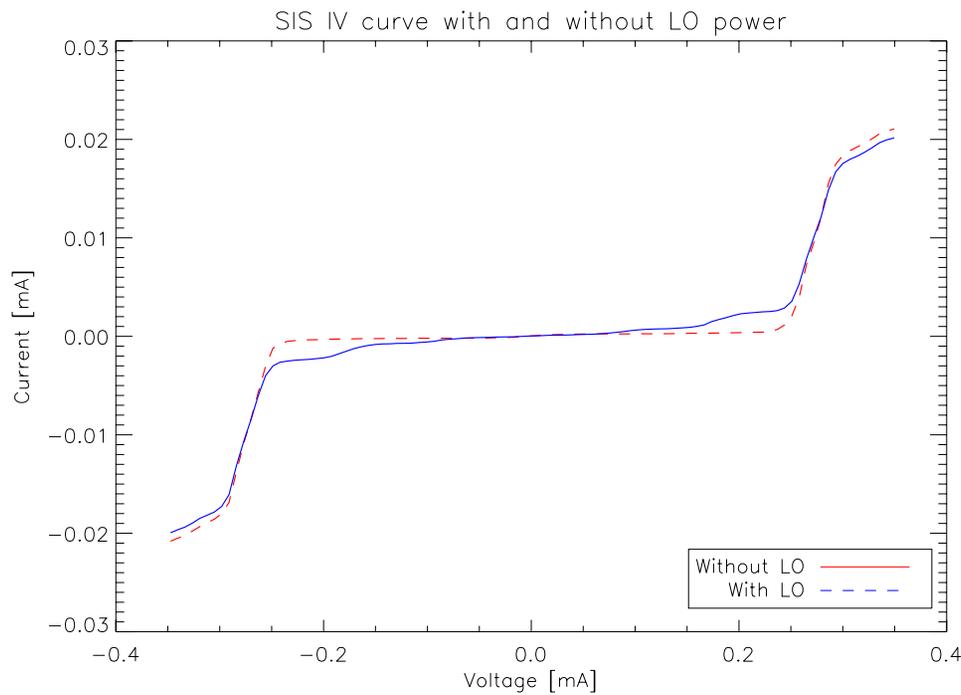




## Detector Block for Phase switch RF tests

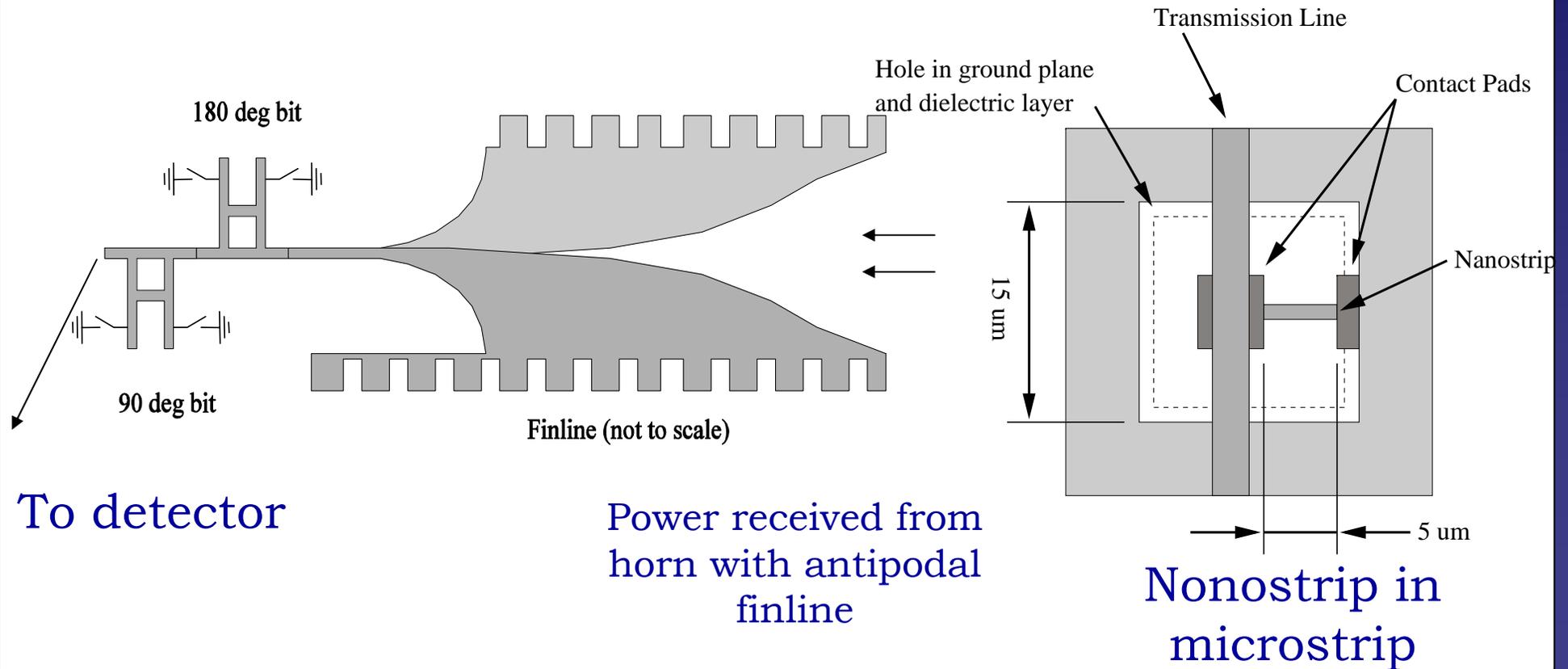






## Phase Modulation work at Oxford...Cont

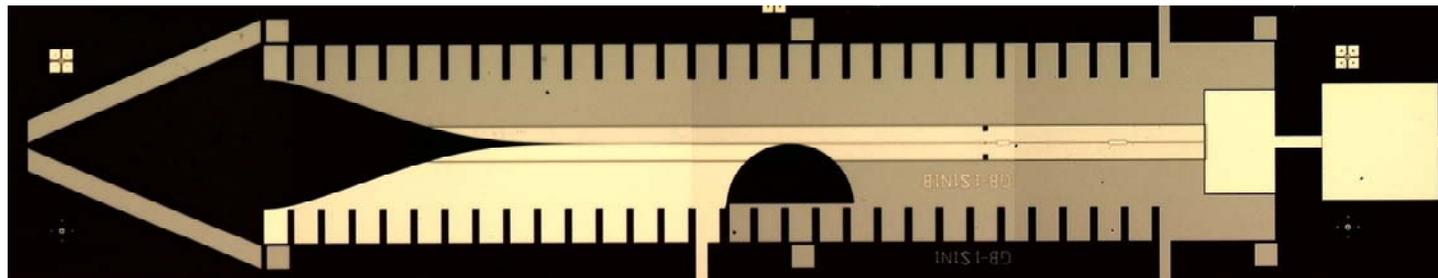
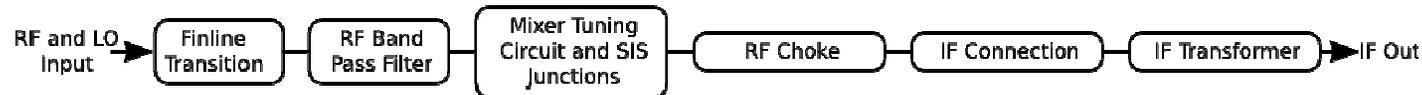
- Stage Three: Integrate nanostrip in microstrip:  
**Designed**



- SIS
  - Very high dynamic range and saturation power
  - Very fast response
  - Cheap readout
  - Easy to integrate with planar circuits
  - Can be used as a direct detector and a Mixer
  - Problem:
    - Suppression of pair tunnelling
    - Shot noise

## 220-GHz Ultra-BroadBand Interferometer for S-Z – GUBBINS

- Single baseline interferometer at 190-260 GHz
- 0.5m baseline, 0.4m primary mirrors (11' primary beam)
- 2x SIS mixers, designed for ultra-wide IF bandwidth
- Single closed cycle cryostat
- Single LO with phase switching in LO optical path
- Very wideband IF system:
  - Wideband, low noise IF amplifiers (initially 3-13 GHz, with upgrades intended)
  - 2-20 GHz analogue sideband separating complex correlator with 16 spectral channels



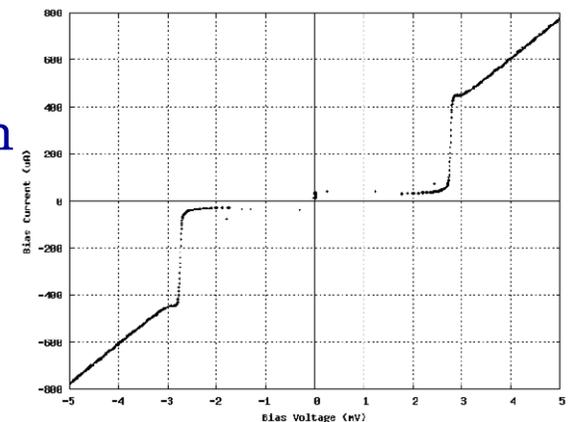
IF bandwidth 2-15 then extend to 20 GHz

Band pass filter to isolate the high IF frequen

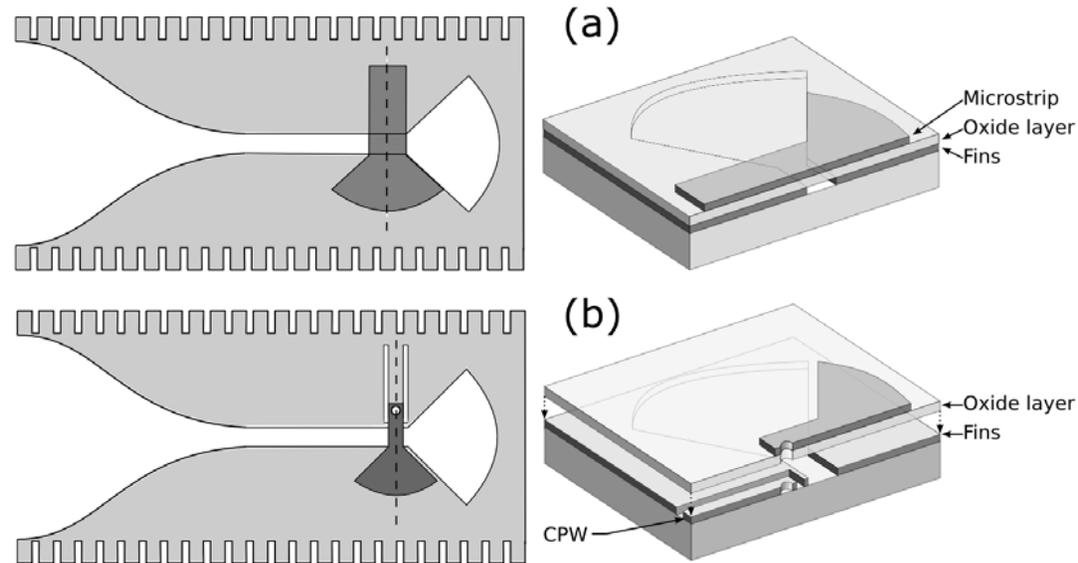
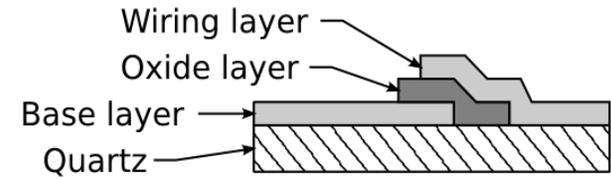
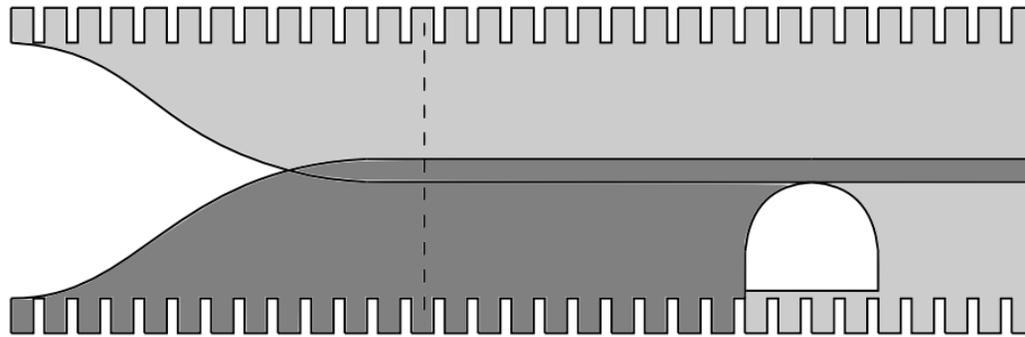
Complex mixer tuning circuits

RF transformer

Grimes *et al*, STT, Groningen



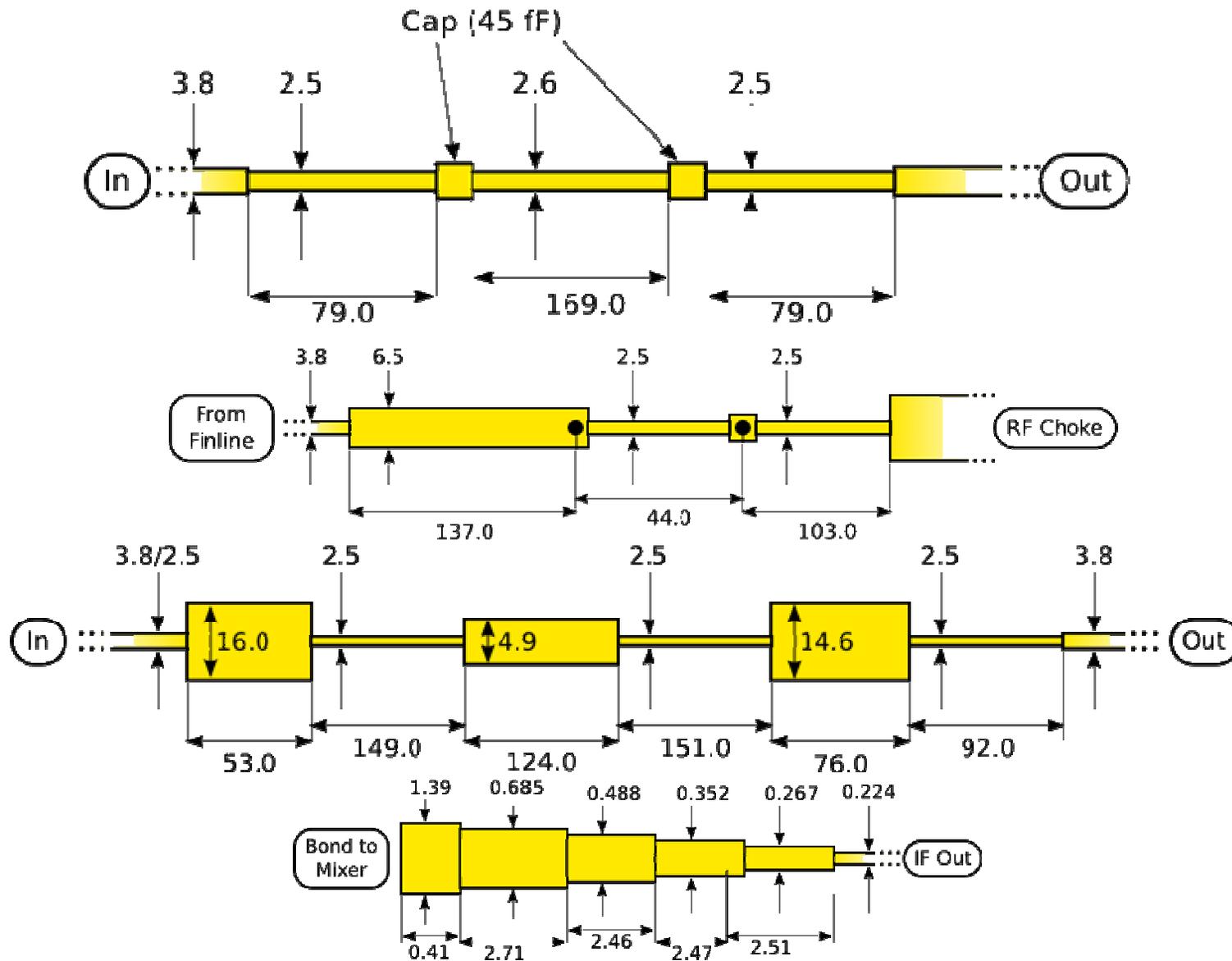
# New Finline Transition



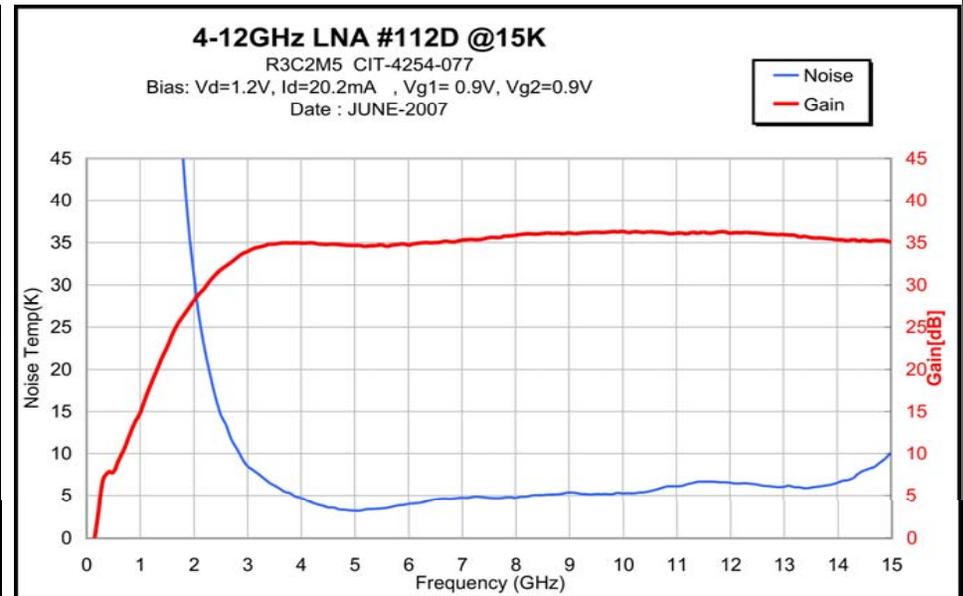
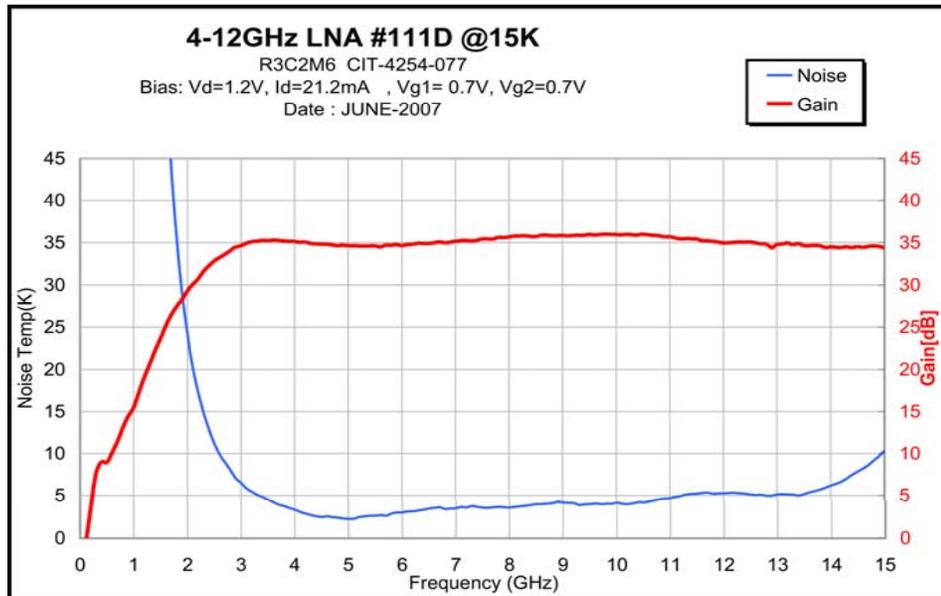
Yassin, et al, *Electron lett.* (in press)

# Mixer circuits

4.3x4.3  
Analysed Nb



- Commercial bias tees
- 3-13 GHz cryogenic IF amps from CalTech (Sander Weinreb)



- 35 dB gain, 4-6 K noise
- Only need two for first version of GUBBINS, but later developments may need more (sideband separating mixers)